

TANANA
Geotechnical



**GEOTECHNICAL INVESTIGATION
ELLER SUBDIVISION ROAD DESIGN
TANANA, ALASKA**

for

**United States Department of the Interior
BUREAU OF INDIAN AFFAIRS
Juneau Area Office
P. O. Box 25520
Juneau, Alaska 99802-5520**

**Rodney P. Kinney Associates, Inc.
1600 Centerfield Drive, Suite 202
Eagle River, Alaska 99577
Phone: (907)694-2332
FAX: (907)694-1807**

October 1992

RODNEY P. KINNEY ASSOCIATES, INC.

CONSULTING ENGINEERS 907/694-2332 FAX 907/694-1807

16600 Centerfield Dr., Suite 202

P.O. Box 771102

Eagle River, Alaska 99577

November 9, 1992

United States Department of the Interior
BUREAU OF INDIAN AFFAIRS
Juneau Area Office
P. O. Box 25520
Juneau, Alaska 99802-5520

Project No. 92-RK-1184B

Attention: Aaron Weston, COR

Subject: ELLER SUBDIVISION
Tanana, Alaska

Gentlemen:

We are pleased to submit the results of our Geotechnical Investigation for the subject project. The field work has been accomplished as of August 21, 1992 as authorized in our contract dated April 27, 1992 (Indefinite Delivery Contract No. CBE00001892003 JO-RD #080-2).

Five copies of this report reproduced on RPKA bond with GBC binding are transmitted with this letter.

The accompanying report presents our recommendations and the study and field results upon which they are based. All work has been accomplished by or under the direct supervision of the undersigned. Please call if you have any questions regarding the contents of the accompanying report.

Very truly yours,
RODNEY P. KINNEY ASSOCIATES, INC.



Rodney P. Kinney, Sr., Ph.D.
C.E.O.

RPK:adt

enclosures



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State of Alaska Material Analysis
Bear Creek and Dredge Stockpile

GEOTECHNICAL INVESTIGATION

SCOPE

This report describes the results of our geotechnical investigation at the subject site. The purpose of this study is to determine the "basement" soil intended to support the proposed roadway, and to present our opinions, conclusions and recommendations for roadway design. A discussion regarding geotechnical site and permafrost conditions as well as frost-susceptibility are also enclosed. A material source study was performed and is also discussed in this report.

DESCRIPTION OF PROJECT

The project will consist of new construction of approximately one mile of roadway within the City of Tanana. Specifically, the project will consist of constructing the subdivision roadbed as shown in Figure 1.

FIELD INVESTIGATION

Three tests were hand-excavated on August 21, 1992 at the locations shown in Figure 1. The test pits were supplemented by hand probes at 50 foot centers on Fourth, Fifth and Sixth Avenues and on Eamole, Yukon and Kapukuk Streets. The field work was done under the observation of our Engineering Technician who visually classified the test pits and samples in the field. Test pit logs have been prepared from the field data and are presented as Figures 2 through 4 inclusive. Our Key to test pit logs is shown as Figure 5. Gradation test results are in Figures 6 and 7. The test pits varied in depth from 1 1/2 feet to 2 feet below the existing ground surface.

LABORATORY TESTING

The laboratory testing program consisted of grain size distribution analyses (ASTM D 422) and Atterberg Limits (ASTM D 4318). The results of the test results are presented in Figures 6 and 7.

SITE AND SOIL CONDITIONS

The topography in the project area is nearly flat to slightly sloping toward the river. Drainage is generally to the south with a shallow swale bordering the east side of the subdivision. The majority of the vegetation along the alignment consists of a thin organic matt with high brush and trees.

Based on our investigation and prior experience, shallow, fine-grain, permafrost exists across the site. There is a thin (6 inches) cover of organic silts (OL/ML) which are probably ice-rich at depth. In any case, the frost classification is F-4 and the active layer (thaw) at time of excavation varied from 18 to 24-inches below present grade.

Excavation refusal was encountered in all of the test pits and is noted in the logs.

GROUNDWATER

At the time of excavation, free ground water was not detected in any of the test pits within the depths explored.

BORROW SITES

We have made inquiries of probable sources of import. The sources are limited and of unknown quality and quantity with the following exceptions:

1. Approximately 800 cubic yards of dredged river gravel is stockpiled near the river's edge and the royalty cost is quoted at \$4.50 per cubic yard. Approximately 3,000 cubic yards (not verifiable) are estimated to be left at the source and royalty costs are quoted to be "more than \$4.50" per yard.
2. The Bear Creek borrow site reportedly is based on visual examination of creek gravels and "they look the same" as the dredged gravels from the Yukon River.
3. We are attempting to get a report from the City of Tanana regarding the Bear Creek material site.
4. Bedrock and other materials from Mission Hill are not durable and do not make a durable road base.
5. There is an abundance of silt (F-4) with a royalty price of \$0.50 per cubic yard. There is a high organic content in much of the silt in this area. A State of Alaska DOT/PF report has looked into borrow sites and that report is appended. It is our understanding that the State is going to Herc in a drill rig for test drilling purposes this coming March, 1993. It is our understanding that they will investigate some of the island sites as possible sources. If correct, it may be advantageous to coordinate with their investigation.

DISCUSSION AND RECOMMENDATIONS

The site is covered by thaw sensitive, frost-susceptible permafrost. These factors must be taken into account for roadway design. The road prism must be as thick as the predicted thaw depth (estimated 5 feet for dry gravel without insulation) and should be non-frost susceptible (NFS) for a minimum maintenance scenario.

If the roadway is built up above grade, cells will be created within each block and drainage must be provided to prevent ponding. A buildup of the roadway prism above existing grade is least expensive but the adjacent lots are relatively depressed in elevation.

SITE PREPARATION AND FILL REQUIREMENTS

1. Excavate and Replace (finished grade near present grade). Areas to be excavated should be stripped of all loose material, organics, and other organics. The excavated thickness will vary along the corridor from 0 to 3 feet. After stripping, the area to be filled should be inspected to determine if additional excavation is required. The final approved excavation should be graded and compacted prior to placement of any fill. All fill material may be placed in maximum loose lift thickness of 8 inches if self propelled vibratory rollers are used or as otherwise approved during construction by the Soil Engineer.
2. Road Prism Above Present Grade. No stripping is required. Fill may be placed over cut brush and organics, left in place.

3. All structural fill should be non-frost-susceptible material (NFS) compacted to 95 percent of the maximum laboratory density as determined by ASTM 1557-D. Non-structural fill may be "classified" and placed and compacted to 90 percent of the maximum laboratory density. Non-frost-susceptible (NFS) is defined as a granular material, 100 passing the 8-inch sieve, and having less than 10 percent passing the No. 200 Sieve, as determined from the minus 3/4-inch fraction. Classified fill should be free of deleterious material and should be approved for use by the Soil Engineer.

It is recommended that all materials used for structural fills, either import or usable on-site material, meet the following requirements:

<u>Sieve Size</u>	<u>Percent Passing</u>		
	<u>Structural (NFS)</u>	<u>Classified (select)</u>	<u>Unclassified</u>
8-inch	100	-----	-----
2-inch	85-100	100	-----
3/4-inch	-----	-----	-----
No. 4	30-70	-----	-----
No. 10	-----	-----	-----
No. 200	0-10*	0-10*	-----
CBR**	≥50	≥10	≥2
P.I.	≤5	≤10	≤15

* As determined from the 3/4-inch fraction.

** California Bearing Ratio

The on-site silts are moisture sensitive and will easily rut under heavily loaded traffic.

In all cases fill, excavation, placement, stockpiling, handling, etc. should be accomplished in a manner that prevents contamination by deleterious substances. Finally, frozen fill material should not be used nor should fill be placed over frozen surfaces. Fill placed within the building limits (as well as undisturbed native soils) should not be allowed to freeze.

4. Cut and fill slopes. The natural undisturbed granular materials at this site range from loose to very dense. Our experience indicated that the undisturbed, short term strengths of these deposits are unpredictable however, and bank failures occur suddenly (mud flows) and without warning. These soils have an angle of response of about 17 to 20 degrees. This angle is safe for unsaturated short term construction slopes of any height, remolded or otherwise, but not for repeated freeze thaw cycles or wet, inclement weather and slope maintenance should be anticipated.

Specific recommendations regarding construction slopes will require analysis for each specific set of conditions at the site. In some cases, shoring may be needed where the excavation is deep. All permanent cut and fill slopes should not be sloped steeper than 2 horizontal to 1 vertical, surface water should be diverted so run-off will not flow over and/or down the face of permanent slopes.

5. Road section. Two requirements must be fulfilled by any roadway section. First, it must resist base shear failure and rutting as a result of lateral movement beneath repeated wheel loads. Second, differential vertical and deflection movements must not exceed the amount permissible for that particular type of surface. Two scenarios can be considered for design:
 - A. A road composed of a 12-inch structural gravel surface (Type B) over a 36-inch classified subbase (Type A). The main objective of the 48-inch section is to minimize frost heave and to maintain the vertical movement requirements mentioned above. In event that additional subbase fill is required, unclassified fill may be used. The classified gravel, select import and unclassified materials should be compacted to 95 percent of the maximum laboratory density. Based on the collected data, it is

believed that this structural section can be used along the entire alignment and will require the least maintenance of the sections considered.

- B. A road composed of a 12-inch classified gravel surface (Type B) with a filter fabric lining over unspecified compactable material adequate to support design loads. The filter fabric should meet the requirements of Section 712.13 of the "Standard Specifications for Construction of Roads and Bridges on Federal Highway Projects", 1985 edition. This scenario would require more maintenance and upkeep because of the frost-susceptibility of the subbase.
 - C. This investigation indicates that the on-site soils are organic silts and are frost susceptible. For best results, they should be removed and replaced with select import to a minimum depth of 3-feet below the recommended classified gravel section. All stripped and excavated surfaces should be compacted and inspected by the Soil Engineer prior to fill placement. The depth of excavation can be reduced provided insulation is utilized as proposed. In this instance, the road prism should be excavated to grade and left exposed for one winter. At the end of winter but prior to thaw, insulation should be placed and NFS placed over the insulation.
6. Cold region considerations. The soils encountered in the test pits for this investigation are highly frost susceptible. These soils may not be used as structural fill material and should be separated and handled accordingly. If frost susceptible soils are exposed at the base of excavations, the Soil Engineer should be consulted for further recommendations that should include minimum extent(s) and depth(s) of removal and replacement. Fill should only be placed over frozen ground that has been properly prepared prior to freezing.
7. Retaining Walls (Culvert Headwalls). Retaining walls that are free to deflect at the top should be designed to resist an active equivalent fluid pressure of 40 pcf plus a uniform pressure of 100 psf. Restrained walls should be designed for a trapezoidal pressure with a maximum intensity of $25 H$ psf where H is the effective height of the retained soil. Starting at the top of the wall, the maximum intensity will occur between 0.2 H -feet and

0.8 H-feet below ground surface with zero intensity at 0 and H-feet below the ground surface. A passive equivalent fluid pressure of 450 pfc and a frictional resistance of 0.5 may be used for design. A minimum safety factor of 1.5 is recommended for design purposes. It is recommended that only NFS soils be placed behind walls that are exposed to winter temperatures. NFS soils should extend for at least a minimum horizontal distance of 10-feet behind walls exposed to freezing.

It is recommended that retaining walls be supported by continuous spread footing foundations bearing on at least 18-inches of N.F.S. undisturbed native soil or well compacted structural fill. Footings may be designed to support maximum allowable bearing pressures of 1,500 pounds per square foot (psf) due to dead load, 2,500 psf due to combined dead plus live load, or 3,500 psf due to all loads, including seismic. At the recommended pressures, footing should extend at least 42-inches below the lowest adjacent grade. Retaining wall footings should have a minimum width of 12-inches.

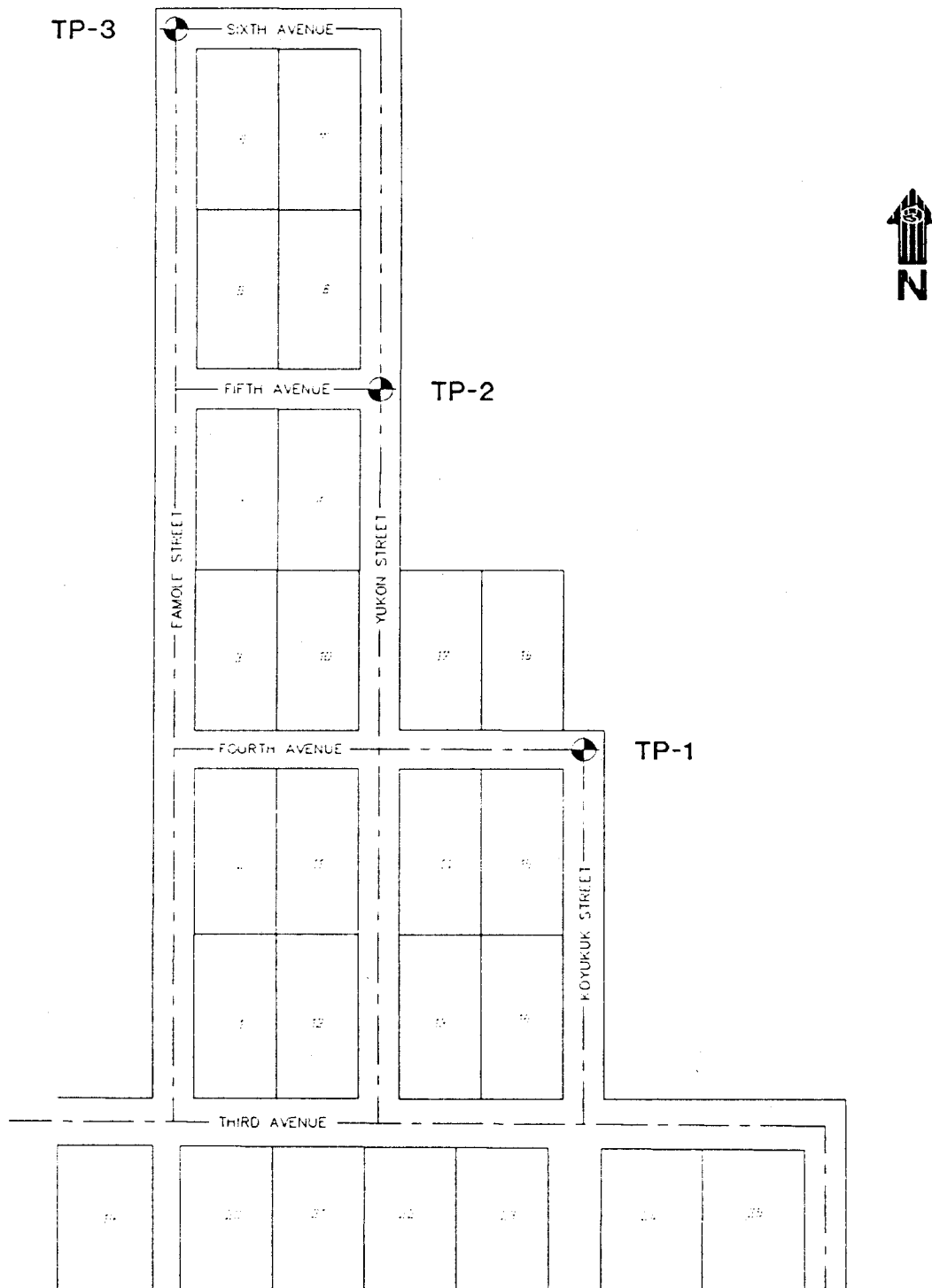
Hand held compaction equipment should not be allowed to compact soils within a horizontal distance of 18-inches from the back face of any retaining wall. In the case of the heavier self propelled vibratory equipment, this distance should be increased to at least 4-feet. Alternatively, the walls may be braced during compaction and the walls designed for the higher transitory impact loads of the compaction equipment.

LIMITATIONS

The recommendations in this report are based on the assumption that soil and water conditions do not deviate appreciably from those disclosed in the test pits. In the event the soils are not consistent with those discussed or variation or undesirable conditions are encountered during construction, Rodney P. Kinney Associates, Inc. should be notified so that supplemental recommendations can be made. Finally, some data and conclusions are based on verbal data that will need substantiation during construction.

FIGURES 1 through 7

TANANA TEST PIT LOCATIONS



TP-1 = TEST PIT LOCATION AND NUMBER

SCALE: 1"=200'

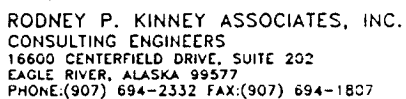
DRAWN BY: MLE

DATE: 10-6-92

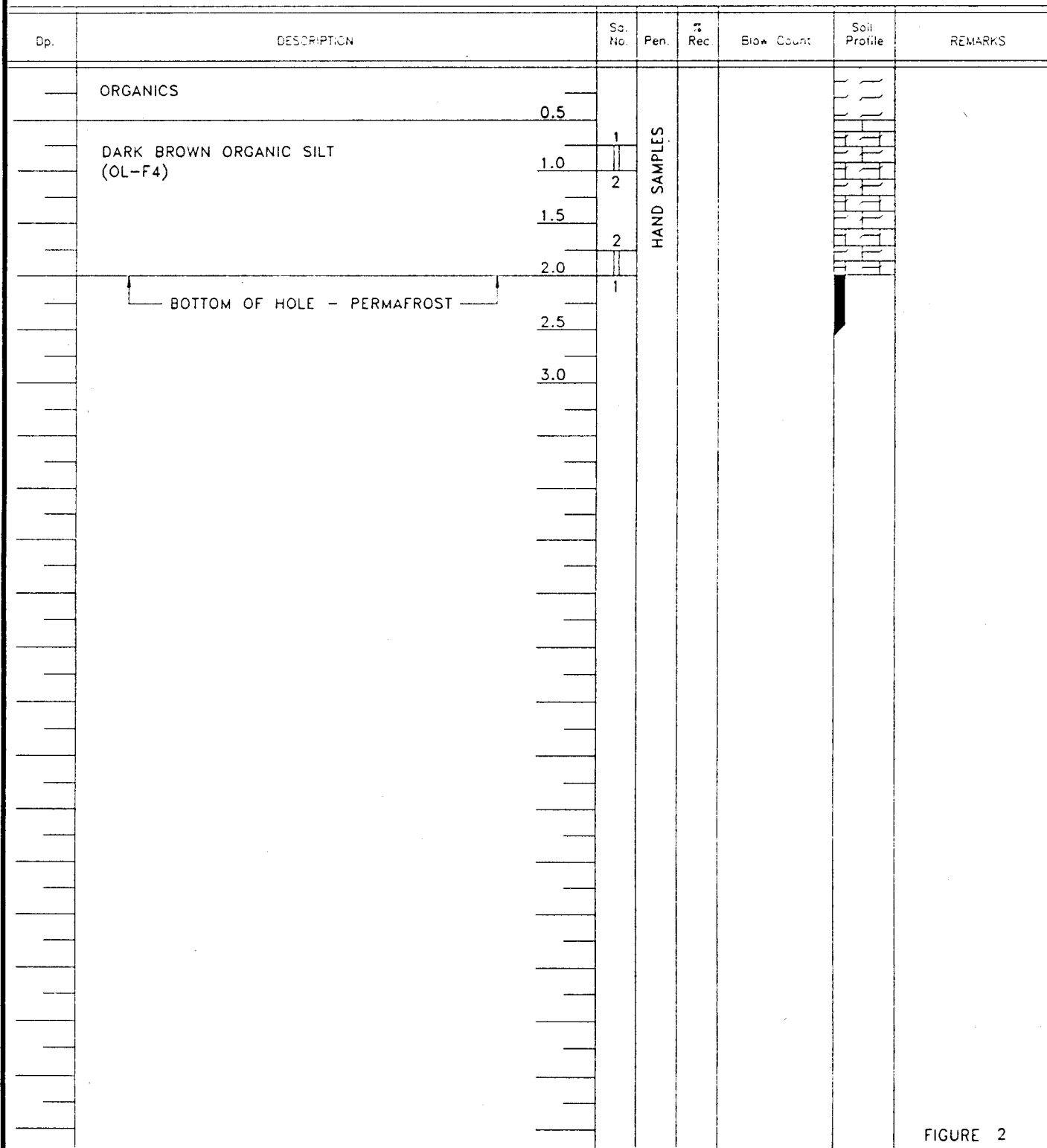


RODNEY P. KINNEY ASSOCIATES, INC.
CONSULTING ENGINEERS
16620 CENTERFIELD DRIVE, SUITE 202
EAGLE RIVER, ALASKA 99577
PHONE: (907) 694-2332 FAX: (907) 694-1807

FIGURE 1



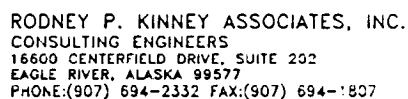
Wt. Hammer: NA



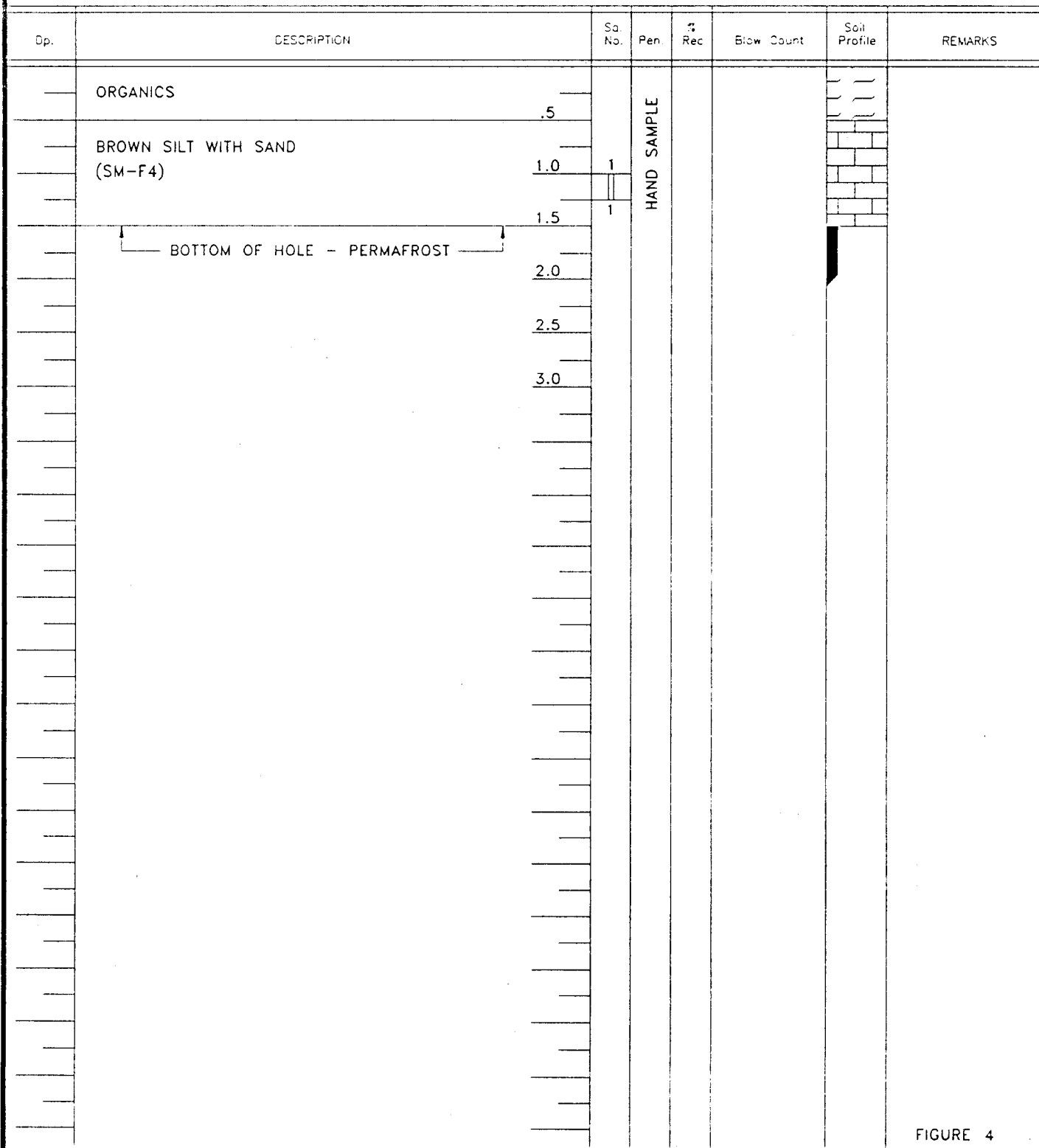


Wt. Hammer: NA

FIGURE 3



Wt. Hammer: NA





RODNEY P. KINNEY ASSOCIATES, INC.
CONSULTING ENGINEERS
16600 CENTERFIELD DRIVE, SUITE 202
EAGLE RIVER, ALASKA 99577
PHONE: (907) 694-2332 FAX: (907) 694-1807

Date: _____

Name: Key To Borings Location: _____

Hole No.: _____ Type of Boring: _____ Rig: _____

Datum: _____ Engineer: _____ Wt. Hammer: _____

Dp.	DESCRIPTION	Sa. No.	Pen.	% Rec.	Blow Count	Soil Profile	REMARKS
	N.F.S. = Non-frost-Suseptible	1					
	Depth below ground surface	2					
		3					
		4					
	Sample No. (increases numerically)	5	1				
	Standard Split Spoon Sampler (2" ϕ O.D. - S.S.)	6	18	80	45		
	Denotes Number of Samples saved	7	1				
	Actual penetration by the Sampler	8					
	Actual length of soil sample retrieved	9					
		10	2				
	Large Sampler with liners (3" ϕ O.D. & Blow count shown is uncorrected)	11			25 40 6 2		
		12	1				
		13					
		14					
		15	3				
	Shelby or other thin walled Sampler	16					
		17	1				
		18					
		19	4				
	Hand Sample	20	1				

Frozen

Blows to drive the Sampler the last 12" of a 18" drive

When unable to drive 18", blow count is shown as recorded. The top number being blows and the bottom is penetration in inches.

Denotes free ground water in boring

ATD = At time of drilling.

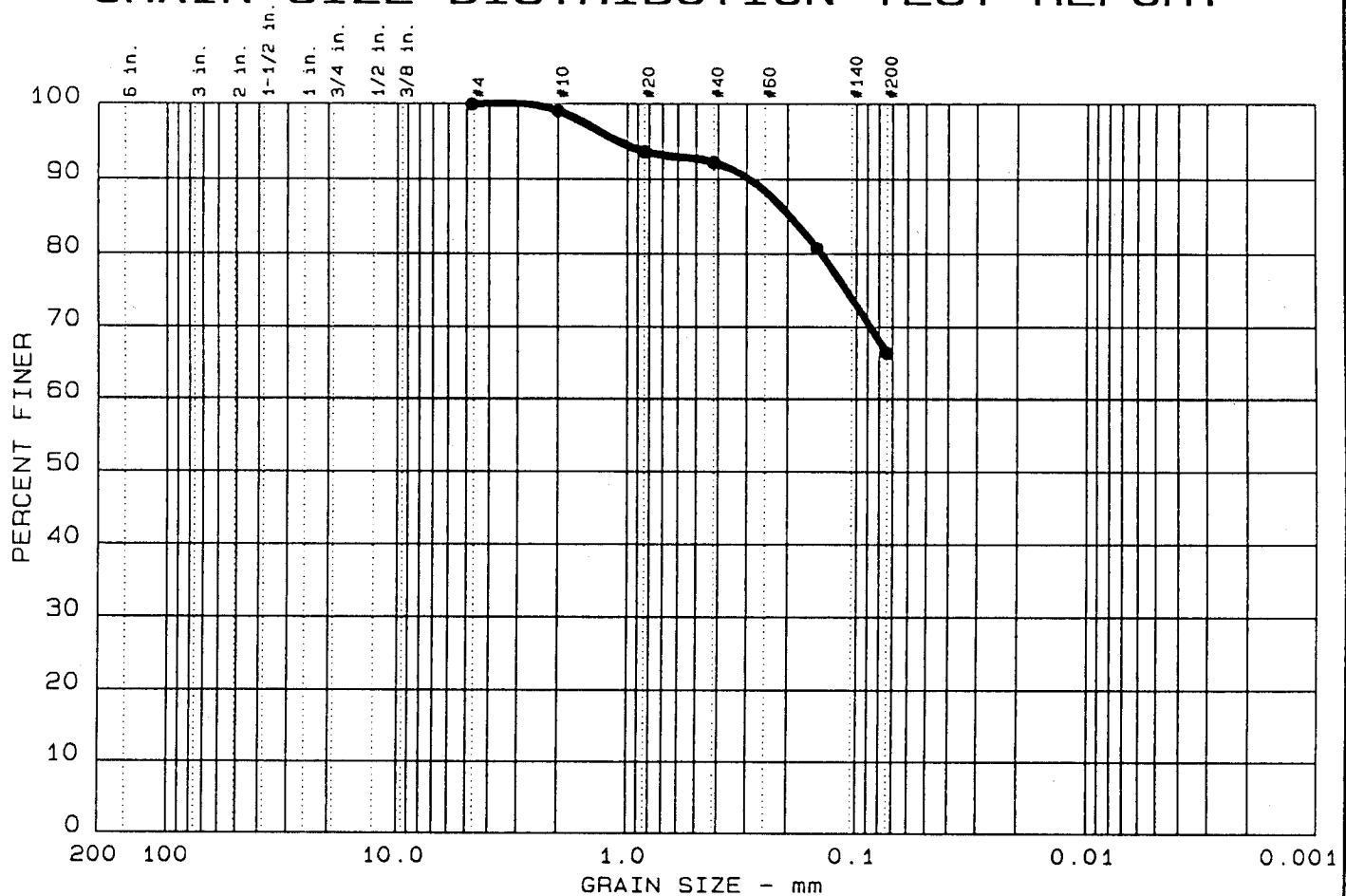
M.C. = Moisture Content in percent.

D.D. = Dry Density in pcf.

0.9 tsf = Lab Torvane Determination

FIGURE 5

GRAIN SIZE DISTRIBUTION TEST REPORT



Test	%+75 mm	% GRAVEL	% SAND	% FINES
● 19	0.0	0.0	33.4	66.6

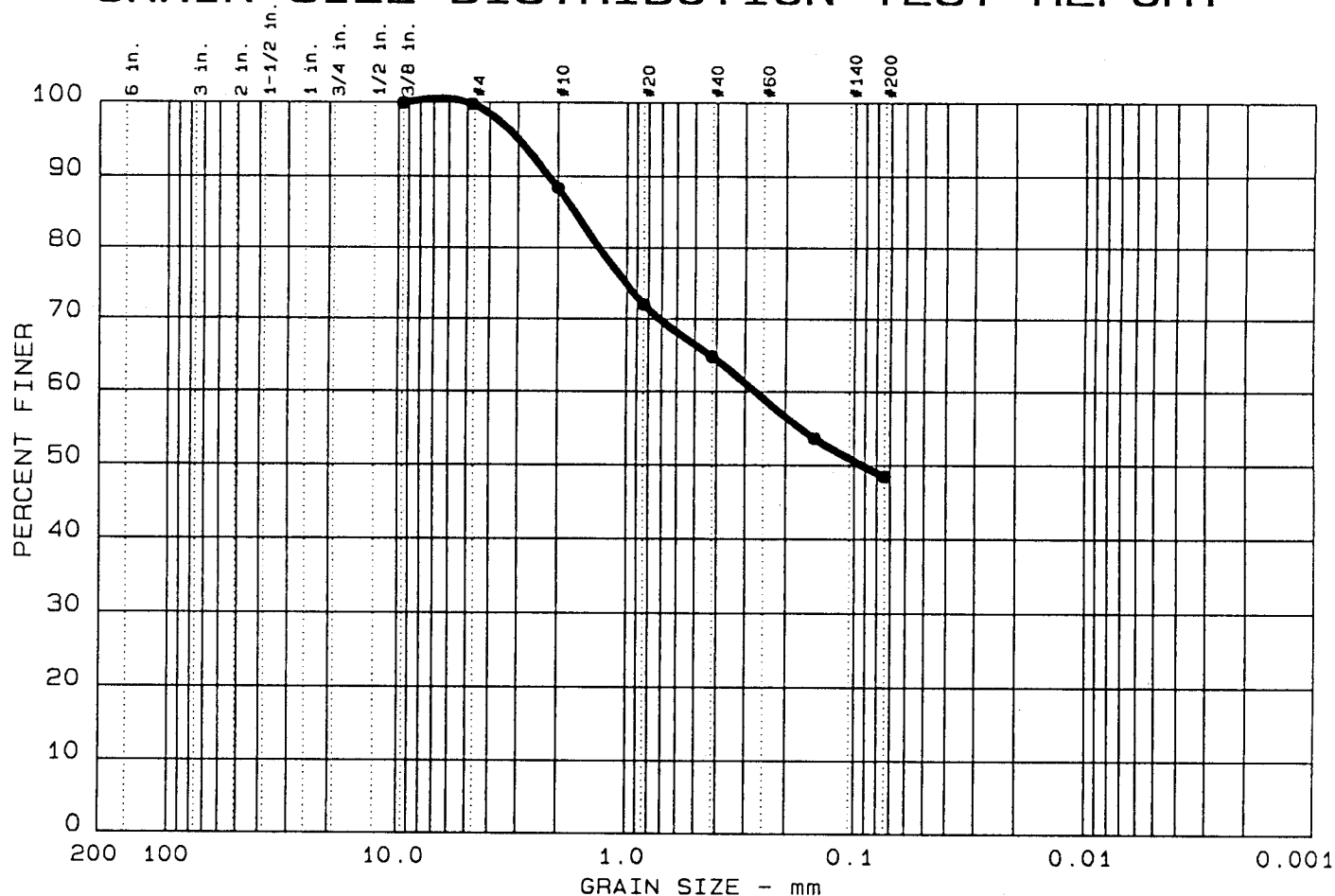
LL	PI	D ₈₅	D ₆₀	D ₅₀	D ₃₀	D ₁₅	D ₁₀	C _c	C _u
●		0.19							

MATERIAL DESCRIPTION	USCS	AASHTO
● ORGANIC SILT	OL	A-4 (0.0)

Project No.: 1184B Project: TANANA ROAD DESIGN ● Location: TH-1, 2.0' Date: 10-16-92	Remarks: FROST CLASS: F4
GRAIN SIZE DISTRIBUTION TEST REPORT RODNEY P. KINNEY ASSOCIATES	

Figure No. 6

GRAIN SIZE DISTRIBUTION TEST REPORT



APPENDIX A

State of Alaska Material Analysis

Bear Creek and Dredge Stockpile

NOV-13-92 TUE 13:03 DOT CONTRACTING FAX NO. 4512353 P. 01
STATE OF ALASKA

DEPARTMENT OF TRANSPORTATION AND PUBLIC FACILITIES
NORTHERN REGION, DESIGN AND CONSTRUCTION

WALTER J. HICKE GOVERNOR

2301 PEGER ROAD
FAIRBANKS, ALASKA 99705-5316
PHONE: (907) 451-2200

FAX #: 694-1807

TO: ROD KEENEY

PHONE: _____

FROM: JOHN D. BENNETT

PHONE: 451-2229

MESSAGE: THE 1992 SAMPLES FROM BEAR CREEK & DREDGE STOCKPILE
ARE STILL BEING RUN - WILL SEND RESULTS WHEN COMPLETE

THE RESULTS OF THIS TESTING ARE ONLY
REPRESENTATIVE OF THE MATERIAL AS SUBMITTED

CHIEF MATERIALS ENGINEER

LAB REPORT

PRECONSTRUCTION	<input type="checkbox"/>	CONSTRUCTION	<input type="checkbox"/>
ACCEPTANCE	<input type="checkbox"/>	QUALITY	<input type="checkbox"/>
ASSURANCE	<input type="checkbox"/>	INFORMATION	<input type="checkbox"/>
		FINAL RECORD	<input type="checkbox"/>

TEST OF AGG. CRUSHED BASE COURSE ITEM NO. 510

PROJECT NO. <u>AIP 3-02-0290-01</u>		ITEM NO. <u> </u>		FINAL RECORD <input type="checkbox"/>	
PROJECT NAME <u>Ralph M. Calhoun Memorial Airport, Tanana</u>		LABORATORY NO. <u>86B-601</u>			
SAMPLED FROM <u>D41812/60457</u>		CRUSHER BELT			
SOURCE <u>Yukon River</u>		SUBMITTED BY <u>Ethan Birkholz</u>		FIELD NO. <u>I-BC-G-3</u>	
LOCATION (RDWY.) <u>Tanana, Alaska</u>		QUANTITY REPRESENTED <u> </u>		DATE <u>Sept 23, 1986</u>	
EXAMINED FOR <u>Conformance</u>		DEPTH <u> </u>		DATE SAMPLED <u>08-29-86</u>	
		SPECIFICATION <u> </u>		DATE RECEIVED <u>09-03-86</u>	

% PASSING SIEVE	AS RECEIVED		SPEC
4"			
3"			
2"			
1 1/2"			
1"	100	100	100
3/4"	100	99	70-100
1/2"	90	88	
3/8"	78	79	
#4	55	58	35-65
#8	41		
#10	39	41	
#16			
#20	30		
#30			
#40	23	20	15-25
#50	19	15	
#80	13	9	
#100	12	8	
#200	8	4.2	5-15
.02MM			
.005MM			

OPTIMUM MOISTURE		
MAX. DRY DENSITY		
MAX. DENSITY NUMBER		
CORR. MAX. DRY DENSITY		
FIELD DENSITY		
FIELD MOISTURE		
% COMPACTION		
% + 3/4"		
% + NO. 4		

AASHO T-190D ☐ ALASKA T-12 ☐

% FRACTURE _____

DEGRADATION VALUE _____

NATURAL DENSITY _____

NATURAL MOISTURE _____

WEIGHT LOOSE _____

WEIGHT RODDED _____

MISCELLANEOUS _____

% + 10"	
% + 3"	
% GRAVEL	
% SAND	
% SILT	
% CLAY	
FSV	
LL	
PL	
PI	
SOIL CLASS	

STATIC IMMERSION

BRAND _____ 0% _____ %%

1% 1½% 2%

DELETERIOUS MATERIALS:

[illegible]

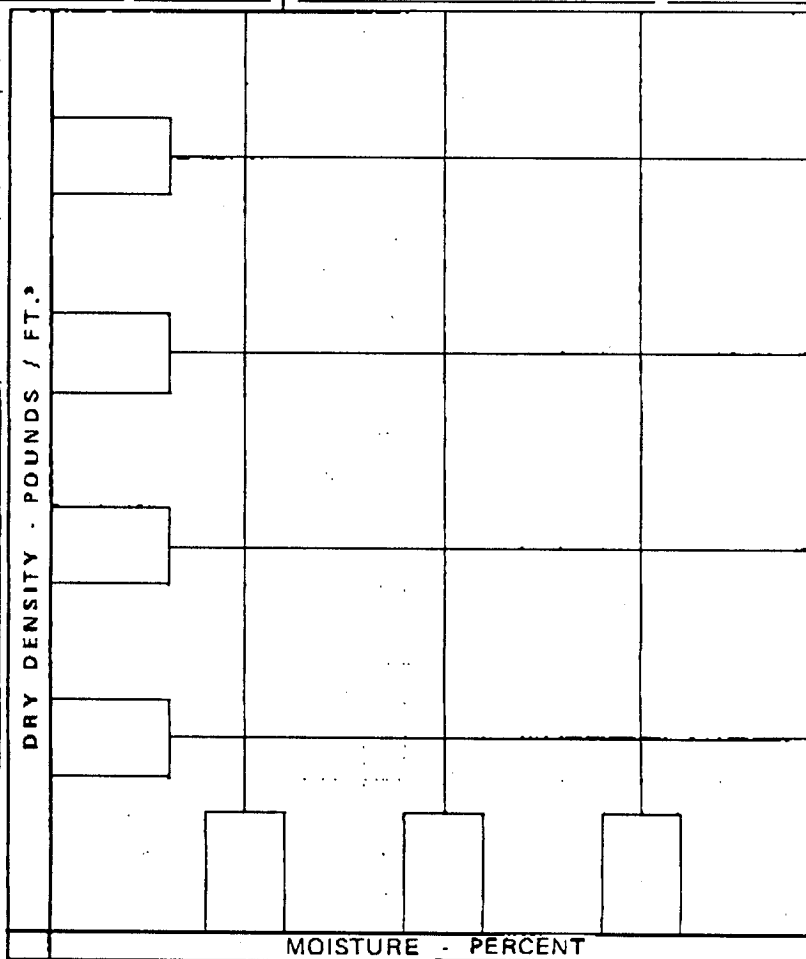
LA, ABRASION LOSS _____ GRADE _____

THIN-ELONGATED _____

ORGANIC COLOR _____ THAN 500 PPM

MORTAR COMPRESSION STRENGTH:

	STANDARD	SAMPLE	RATIO	SPEC
_____ DAY, PSI	_____	_____	_____	_____
_____ DAY, PSI	_____	_____	_____	_____



FOR ROAD MATERIALS LABORATORY USE ONLY

WHEN PROCESSED TO CONFORM TO GRADING REQUIREMENTS. THIS MATERIAL IS SATISFACTORY FOR

AGG. CRUSHED BASE COURSE

CONFORM TO SPECIFICATIONS:
YES ☒ NO ☐ N.A. ☐

SIGNATURE Paul W. Misterek
Paul W. Misterek, SMC

TITLE

CHIEF MATERIALS ENGINEER

LAB REPORT

PRECONSTRUCTION ☐ CONSTRUCTION ☒

ACCEPTANCE ☒ QUALITY ☒

ASSURANCE ☐ INFORMATION ☐

FINAL RECORD ☐

TEST OF BORROW EMBANKMENT

ITEM NO. 330c

PROJECT NO. AIP-3-02-0290-01

PROJECT NAME Tanana R/W Improvements

LABORATORY NO. 86B-625

SAMPLED FROM D41812/60457 Runway

SUBMITTED BY K. Shrewsbury

FIELD NO. 0-1/BX-SPD-1CK

SOURCE Yukon River

QUANTITY REPRESENTED

DATE Sept 23, 1986

LOCATION (RDWY.) Sta 48+00, 135' Rt

DEPTH -10

DATE SAMPLED 09-03-86

EXAMINED FOR Quality, T180D, T-12

SPECIFICATION

DATE RECEIVED 09-08-86

% PASSING SIEVE	AS RECEIVED	FIELD	SPEC.		SPEC.		SPEC.
4"				OPTIMUM MOISTURE	4.3		
3"	100	100		MAX. DRY DENSITY	143.1		
2"	95	97		MAX. DENSITY NUMBER			
1 1/2"	89	89		CORR. MAX. DRY DENSITY			
1"	78	82		FIELD DENSITY			
3/4"	71	77		FIELD MOISTURE			
1/2"	61	66		% COMPACTION			
3/8"	54	58		% + 1/2"			
#4	39	42		% + NO. 4			
#8	29			AASHTO T180D <input type="checkbox"/> ALASKA T-12 <input type="checkbox"/>			
#10	28	30		% FRACTURE			
#16				DEGRADATION VALUE	68		
#20	22			NATURAL DENSITY			
#30				NATURAL MOISTURE			
#40	16	18		WEIGHT LOOSE			
#50	12	34		WEIGHT RODDED			
#80	7	20		MISCELLANEOUS			
#100	6			BULK	2.71		
#200	4	4.2		SSD	2.73		
.02MM				APP	2.76		
.005MM				STATIC IMMERSION			
DUST RATIO:				BRAND	0% 1% 2%		

DELETERIOUS MATERIALS:

MINUS #200 MESH

SOFT FRAGMENTS

COAL & LIG. OR LT. WT. PART.

CLAY LUMPS

STICKS & ROOTS

FRIABLE PARTICLES

SPECIFIC GRAVITY

ABSORPTION

FINESS MODULUS

SULFATE SOUNDNESS

FREEZE-THAW RATIO

L.A. ABRASION LOSS 23% GRADE A

THIN-ELONGATED

ORGANIC COLOR

THAN 500 PPM

MORTAR COMPRESSION STRENGTH:

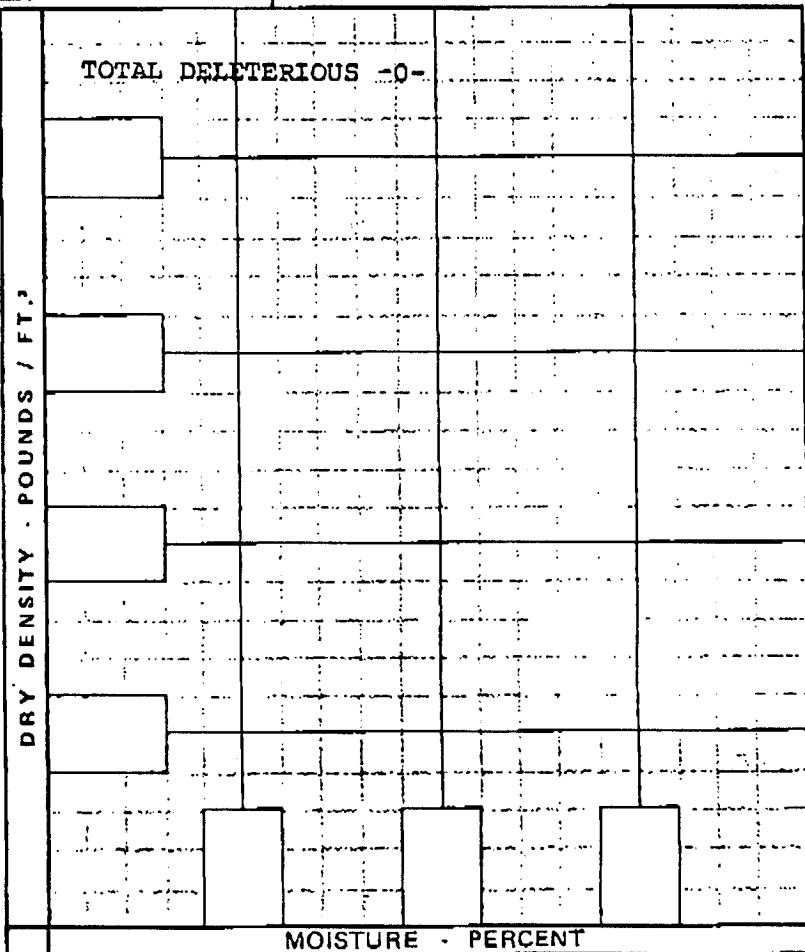
STANDARD SAMPLE RATIO SPEC

DAY, PSI

DAY, PSI

DESCRIPTION OF MATERIALS:

REMARKS:



FOR ROAD MATERIALS LABORATORY USE ONLY

WHEN PROCESSED TO CONFORM TO GRADING REQUIREMENTS, THIS MATERIAL IS SATISFACTORY FOR:

BORROW EMBANKMENT

CONFORM TO SPECIFICATIONS: YES ☐ NO ☐ N.A. ☐

SIGNATURE Paul W. Misterek, SMI

STATE OF ALASKA

DEPARTMENT OF HIGHWAYS

DH-209

PRECONSTRUCTION ☐ CONSTRUCTION ☒

FIELD CONTROL ☐ QUALITY ☐

CHECK ☒ PROGRESS RECORD ☐

INFORMATION ☐ FINAL RECORD ☐

TEST OF BORROW EMBANKMENT

ITEM NO 330c

PROJECT NO. 30173842 PROJECT NAME Tanana R/W Improvements LABORATORY NO. 86B-625

SAMPLED FROM Sta 48 - 135' Rt SUBMITTED BY Ken Shrewsbury FIELD NO. BX-SDP-1ck

SOURCE Yukon River QUANTITY REPRESENTED Source DATE Sept 15, 1986

ROADWAY LOCATION DEPTH DATE SAMPLED 09-03-86

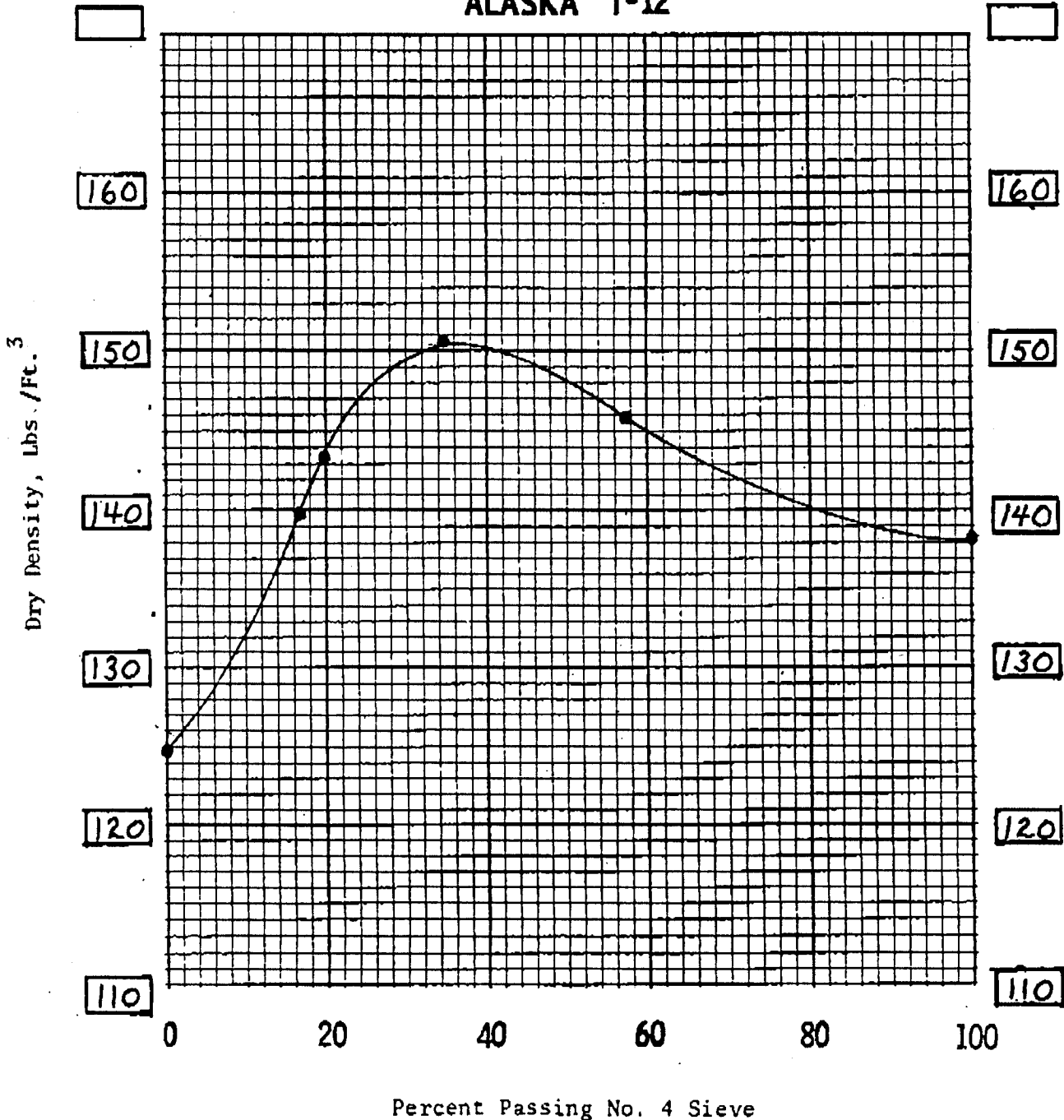
EXAMINED FOR T-12 SPECIFICATION DATE RECEIVED 09-08-86

SPECIFIC GRAVITY
+ No. 4 2.76

RESULTS OF VIBRATORY COMPACTION

SPECIFIC GRAVITY
-No. 4 2.69

ALASKA T-12



SIGNATURE

TITLE Materials Engineer

**STATE OF ALASKA - NORTHERN REGION
DEPARTMENT OF TRANSPORTATION AND PUBLIC FACILITIES**

REGIONAL LAB REPORT

PROJECT NAME:	TANANA RUNWAY	LAB #:	87-151
PROJECT #:	30173842	FIELD #:	A-BC-SDP-1
TEST OF:	SURFACE COURSE	DATE SAMPLED:	6-26-87
ITEM #:		DATE RECEIVED:	6-29-87
		DATE TESTED:	7-7-87
SAMPLED FROM:	RUNWAY @ VARIOUS LOCATIONS	ACCEPTANCE:	
DEPTH:		ASSURANCE:	XXXX
SOURCE:		QUALITY:	
QUANTITY REPRESENTED:	SOURCE	INFORMATION:	

SIEVE SIZE	AS REC'D	FIELD SPLIT	SPEC		AS REC'D	SPEC
4"				LL	NV	
3"				PL	NP	
2"				PI	NP	
1 1/2"						
1"	100					
3/4"	100			% FRACTURE:	73	
1/2"	90					
3/8"	81					
#4	60					
#8	48			MAX DENSITY	143.9	
#10	46					
#16				OPTIMUM MOIST	5.3	
#20	37					
#30						
#40	31					
#50	27				COARSE	FINE
#60						
#80	21			SP GR (APP):	2.75	2.73
#100	19					
#200	14		10-15			
.02MM						
.005MM						

* +3":

* ORGANICS:

* NATURAL MOISTURE:

* DELETERIOUS: 0

REMARKS:

CONFORMS TO SPECIFICATIONS:

YES: / NO: NA:

SIGNATURE:

Paul W. Misterek
PAUL W. MISTEREK, RME

STATE OF ALASKA
DEPARTMENT OF TRANSPORTATION
AND
PUBLIC FACILITIES

SOILS TESTING REPORT

CHECK ONE

☒ CENTERLINE

PROJECT NAME & NO. Tanana Airport D-41811

☐

MATERIALS SITE: NO.

SAMPLED BY: G. Brazo

STATION	9+00	13+00	13+00	16+25	16+25	19+25	19+25	22+25
OFFSET (FEET)	25 L	60 R	60 R	60 L	60 L	45 R	45 R	40 L
DEPTH (FEET)	3-7	3-4	6-7	3-4	5-6	0-1.5	2-3	0-1
TEST HOLE NO.	80-1	80-2	80-2	80-3	80-3	80-4	80-4	80-5
FIELD NO.	A	B	C	D	E	F	G	H
LAB NO.	80A-3463	80A-3464	80A-3465	80A-3466	80A-3467	80A-3468	80A-3469	80A-3470
DATE	18 NOV 80	18 NOV 80	18 NOV 80	19 NOV 80	19 NOV 80	19 NOV 80	19 NOV 80	19 NOV
ESTIMATED 1/10"								
" 1/3" to 10"								
PERCENT PASSING	3"							
	2"							
	1"					100		100
	3/4"	100				99		98
	1/2"	99				98		96
	3/8"	99				95		86
	# 4	97				78		78
	#10	97				62		60
	#40	93				49		47
	#50	77				37		35
	#100	77				33		30
	#200	48				26		23
	.02mm	17				22		18
	.005mm	-				12		11
LIQUID LIMIT	NV					NV		NV
PLASTIC INDEX	NP					NP		NP
SOIL CLASS	Gm					SM		Gm
SOIL DESCRIPTION	SaSi	Si	SaSi	Si	Org.Si	SiSaGr	Org.Si	SiSaGr
NAT. MOISTURE		12.1	7.6	12.0	20.7		27.4	
Sp.G. Fine	2.69					2.68		
Sp.G. Coarse								2.68
Absorption								
Max. Density								
Opt. Moisture								
L.A. Abrasion								
Degradation								
Sult. Soundness								
Organics								

* Drill Cuttings F-4

F-3

F-3

NOV-3-82 10E 15:07

DOI CONSTRUCTION

FAH NO. 4012353

F.U.I

STATE OF ALASKA
DEPARTMENT OF TRANSPORTATION
AND
PUBLIC FACILITIES

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CENTERLINE

PROJECT NAME & NO. Tanana Airport D-41811

MATERIALS SITE: NO. _____

SAMPLED BY: G. Brazo

STATION	22+25	25+25	25+25	28+25	28+25	31+25	31+25	34+25
OFFSET (FEET)	40 L	35 R	35 R	35 L	35 L	60 R	60 R	35 L
DEPTH (FEET)	2-3	2-3	6-7	0-1.5	2.5 - 3.5	2-3	4-5	1.5 - 3.0
TEST HOLE NO.	80-5	80-6	80-6	80-7	80-7	80-8	80-8	80-9
FIELD NO.	I	J	K	L	M	N	O	P
LAB NO.	80A-3471	80A-3472	80A-3473	80A-3474	80A-3475	80A-3476	80A-3477	80A-3478
DATE	19 NOV 80	19 NOV 80	19 NOV 80	20 NOV 80	20 NOV 80	20 NOV 80	20 NOV 80	20 NOV 80
ESTIMATED 1/10"								
" 1/3" to 10"								
PERCENT PASSING	3"							
	2"							
	1"			100				
	3/4"	100		99				
	1/2"	99		96				
	3/8"	99		89				
	# 4	97		81				100
	#10	95		64				99
	#40	92		47				97
	#50	89		34				95
	#100	80		29				92
	#200	64		22				85
	.02mm	-		16				78
	.005mm	-		9				-
LIQUID LIMIT	NV			NV				25
PLASTIC INDEX	NP			NP				NP
SOIL CLASS	ML			SM				ML
SOIL DESCRIPTION	SaSi	Org. Si	Si	SiSaGr	Si	Org. Si	Si	Si
NAT. MOISTURE		20.8	16.0		19.0	25.3	21.5	
Sp.G. Fine				2.68				
Sp.G. Coarse								
Absorption								
Max. Density								
Opt. Moisture								
L.A. Abrasion								
Degradation								
Sult. Soundness								
Organics								

* Drill Cuttings

P. 03

FAX NO. 4512353

DUI CONIRHULING

NOV-3-92 TUE 13:08

STATE OF ALASKA
DEPARTMENT OF TRANSPORTATION
AND
PUBLIC FACILITIES

SOILS TESTING REPORT

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CENTERLINE

PROJECT NAME & NO. Tanana Airport D-41811

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MATERIALS SITE: NO.

SAMPLED BY: G. Brazo

STATION	34+25	37+25	40+25	40+25	43+25	46+25	49+25	49+25
OFFSET (FEET)	35 L	30 R	45 L	45 L	30 R	40 L	35 R	35 R
DEPTH (FEET)	5-6	0-1.5	1.5-2.5	3-4	0-2	3-4	0-2	4-5
TEST HOLE NO.	80-9	80-10	80-11	80-11	80-12	80-13	80-14	80-14
FIELD NO.	Q	R	S	T	U	V	W	X
LAB NO.	80A-3479	80A-3480	80A-3481	80A-3482	80A-3483	80A-3484	80A-3485	80A-3486
DATE	20 NOV 80	20 NOV 80	20 NOV 80	20 NOV 80	20 NOV 80	20 NOV 80	20 NOV 80	20 NOV 80
ESTIMATED %±10"								
" ± 3" to 10"								
PERCENT PASSING	3"							
	2"							
	1"							
	3/4"	100			100			
	1/2"	98			99		100	
	3/8"	92			96		98	
	# 4	85			92		95	
	#10	66			77		84	
	#40	51			61		71	
	#50	34			40		53	
	#100	28			35		48	
	#200	20			25		38	
	.02mm	93			19		27	
	.005mm	16			12		18	
		10						
LIQUID LIMIT	NV	NV			NV		NV	
PLASTIC INDEX	NP	NP			NP		NP	
SOIL CLASS	ML	SM			SMd		SM	
SOIL DESCRIPTION	Si	SiSaGr	Si	Org.Si	SiGrSa	Si	SiGrSa	Org.si
NAT. MOISTURE	20.3		18.6	25.0		16.3		22.0
Sp.G. Fine		2.68			2.70		2.70	
Sp.G. Coarse								
Absorption								
Max. Density								
Opt. Moisture								
L.A. Abrasion								
Degradation								
Sult.Soundness								
Organics								

* Drill Cuttings

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SOILS TESTING REPORT

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PROJECT NAME & NO. Tanana Airport D-41811

☐ MATERIALS SITE: NO. _____

SAMPLED BY: G- Brazo

STATION	53+25	57+25	57+25	60+00	63+00	49+00	46+00	
OFFSET (FEET)	40 L	30 R	30 R	50 L	50 R	400 R	350 R	
DEPTH (FEET)	2-3	0-2	6-7	2-3	2-4	2-3	2-3	
TEST HOLE NO.	80-15	80-16	80-16	80-17	80-18	80-22	80-24	
FIELD NO.	Y	Z	AA	BB	CC	DD	EE	
LAB NO.	80A-3487	80A-3488	80A-3489	80A-3490	80A-3491	80A-3492	80-3493	
DATE	21. NOV 80	21 NOV 80	21 NOV 80	21 NOV 80	21 NOV 80	21 NOV 80	22 NOV 80	
ESTIMATED 2+10"								
" & 3" to 10"								
PERCENT PASSING	3"							
	2"	100						
	1"	99						
	3/4"	99						
	1/2"	97						
	3/8"	85						
	# 4	69						
	#10	55			100			
	#40	37			99			
	#50	32			99			
	#100	25			98			
	#200	19			93			
	.02mm	12			-			
	.005mm	-			-			
LIQUID LIMIT		NV			24			
PLASTIC INDEX		NP			NP			
SOIL CLASS		GMd			ML			
SOIL DESCRIPTION	Si	SiSaGr	Si	Si	Si	Org.Si	Si	
NAT. MOISTURE	12.2		27.5	28.6		36.8	13.8	
Sp.G. Fine		2.69						
Sp.G. Coarse								
Absorption								
Max. Density								
Opt. Moisture								
L.A. Abrasion								
Degradation								
Sult. Soundness								
Organics								

* Drill Cuttings

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STATE OF ALASKA
DEPARTMENT OF TRANSPORTATION
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PROJECT NAME & NO. Tanana Airport D-41811

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MATERIALS SITE: NO.

Yukon River

SAMPLED BY:

Miller/Grahek

STATION									
OFFSET (FEET)									
DEPTH (FEET)									
TEST HOLE NO.									
FIELD NO.		84-0190	84-0191	84-2008	84-2009				
LAB NO.		84B-0190	84B-0191	84B-2008	84B-2009				
DATE		6-84	6-84	14 SEPT 84	14 SEPT 84				
ESTIMATED $\pm 10"$									
" $\pm 3"$ to 10"		13							
PERCENT PASSING	3"	100		100					
	2"	94	100	98	100				
	1"	86	97	87	96				
	3/4"	77	93	80	92				
	1/2"	59	80	69	78				
	3/8"	48	73	61	64				
	# 4	28	57	44	38				
	#10	16	47	28	30				
	#40	6	35	-	-				
	#50	-	-	9	11				
	#100	2	19	3	4				
	#200	1	15	2	1				
	.02mm								
	.005mm								
LIQUID LIMIT		NV	NV	NV	NV				
PLASTIC INDEX		NP	NP	NP	NP				
SOIL CLASS		SW	Gmd	GW	GW				
SOIL DESCRIPTION		SaGr	SiSaGr	SaGr	SaGr				
NAT. MOISTURE									
Sp.G. Fine				2.68	2.69				
Sp.G. Coarse									
Absorption									
Max. Density				135.2	135.7				
Opt. Moisture				4.3	5.1				
L.A. Abrasion				22A	24A				
Degradation		69	81	75	77				
Sult. Soundness				4.6					
Organics									

* Drill Cuttings

STATE OF ALASKA
DEPARTMENT OF TRANSPORTATION
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PUBLIC FACILITIES

SOILS TESTING REPORT

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CENTERLINE

PROJECT NAME & NO. Tanana Airport D-41811

☒

MATERIALS SITE: NO. East of Village

SAMPLED BY: G. Brazo

STATION							
OFFSET (FEET)							
DEPTH (FEET)	1.5-7.0	0-7	6-12	BULK			
TEST HOLE NO.	80-31	80-32	80-33	80-34			
FIELD NO.	FF	GG	HH	-			
LAB NO.	80A-3494	80A-3495	80A-3496	81A-81			
DATE	23 NOV 80	23 NOV 80	23 NOV 80	23 NOV 80			
ESTIMATED $\pm 10"$							
" $\pm 3"$ to 10"							
PERCENT PASSING	3"						
	2"	100	100	100	100		
	1"	99	96	92	96		
	3/4"	98	88	83	92		
	1/2"	96	72	67	86		
	3/8"	90	59	57	81		
	# 4	84	37	41	70		
	#10	62	26	32	61		
	#40	46	14	23	25		
	#50	36	11	15	19		
	#100	23	7	6	11		
	#200	14	4	4	8		
	.02mm	7	-	-	3		
	.005mm	-	-	-	-		
LIQUID LIMIT	NV	NV	NV	NV			
PLASTIC INDEX	NP	NP	NP	NP			
SOIL CLASS	SMd	GW	Gw	SW-SM			
SOIL DESCRIPTION	SiGrSa	SaGr	SaGr	GrSa			
NAT. MOISTURE							
Sp.G. Fine	2.68			2.72			
Sp.G. Coarse				2.71			
Absorption				0.7			
Max. Density							
Opt. Moisture							
L.A. Abrasion				27A			
Degradation				79			
Sult. Soundness				1.7			
Organics							

* Drill Cuttings F-3

F-2