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of **ALASKA**  
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October 6, 2025

Dan Opalski  
Deputy Regional Administrator  
Environmental Protection Agency, Region 10  
1200 Sixth Avenue, Suite 155  
Seattle, WA 98101

Subject: Alaska Regional Haze Second Implementation Period State Implementation Plan  
Clarification Memo

Dear Deputy Administrator Opalski,

On July 25, 2022, the Alaska Department of Environmental Conservation (DEC) submitted a State Implementation Plan (SIP) to the Environmental Protection Agency (EPA) to address the visibility protection requirements of Clean Air Act section 169A and 169B and the Regional Haze Rule requirements of 40 CFR 51.308 for the second implementation period. EPA has not yet acted on that submission. The 2022 Regional Haze SIP Submission included the following:

- Calculations of baseline, current, and natural conditions, progress to date, and the uniform rate of progress;
- Long-term strategy for regional haze, including the state's considerations of the costs of compliance, the time necessary for compliance, the energy and non-air quality environmental impacts of compliance, the remaining useful life of any potentially affected anthropogenic source of visibility impairment, a description of the criteria the state used to determine which sources or groups of sources it evaluated, and a description how the four factors were taken into consideration in selecting measures;
- Reasonable progress goals;
- Monitoring strategy for measuring, characterizing, and reporting of regional haze visibility impairment;
- Progress report;
- Determination of adequacy of the existing implementation plan; and
- Description of how the state addressed any comments provided by the Federal Land Managers and procedures for continuing consultation between the state and Federal Land Managers on the implementation of the visibility protection program.

With respect to the long-term strategy, DEC acknowledges that the 2022 Regional Haze SIP Submission relied in part on sulfur dioxide (SO<sub>2</sub>) best available control technology (BACT) analyses and determinations for certain facilities and units originally submitted as part of the Fairbanks North Star Borough 2006 24-Hour PM<sub>2.5</sub> Serious Area and the 189(d) Plan submission made on December 13, 2019 and December 15, 2020, respectively. However, DEC subsequently revised the original SO<sub>2</sub> BACT analyses to address EPA concerns detailed in its proposed disapproval action on January 10, 2023 (88 FR 1454) and to account for more recent vendor quotes and fuel prices. These updated SO<sub>2</sub> BACT analyses were later submitted through the public process by DEC to EPA as part of a December 4, 2024 revision to the Fairbanks North Star Borough (FNSB) Serious Nonattainment Area (NAA) PM<sub>2.5</sub> SIP. The SIP is available at <https://www.regulations.gov/document/EPA-R10-OAR-2024-0595-0078> for docket no. EPA-R10-OAR-2024-0595.

The 2022 Regional Haze SIP submission, as augmented by the December 4, 2024 SIP submission and clarified below, meets the requirements of sections 169A and 169B of the Clean Air Act and 40 CFR 51.308 for the second implementation period. Therefore, DEC is rescinding its June 3, 2025 conditional approval request, and DEC will not revise its SIP by submitting a Supplemental Regional Haze SIP Submission as described in that letter. DEC is sending this letter to make clear that it is the State's intention to rely on the updated BACT analyses for purposes of the Regional Haze SIP.

**Clarifications from DEC's December 4, 2024, Fairbanks North Star Borough Nonattainment Area PM<sub>2.5</sub> (FNSB NAA PM<sub>2.5</sub>) SIP Submission, and July 25, 2022, Regional Haze SIP Submission**

Regarding University of Alaska Fairbanks (UAF) Campus:

- The July 25, 2022 Regional Haze SIP submission used 2017 emissions inventory data to select sources for further analysis. However, the submission did not consider that in 2019 the original coal-fired boilers at this facility were decommissioned and replaced with a modern circulating fluidized bed coal-fired boiler equipped with a limestone injection system which controls SO<sub>2</sub> emissions.
- DEC has determined that current, actual emissions of SO<sub>2</sub> from this facility are so low that the facility screens-out of additional review based on the Quantity over distance (Q/d) source selection methodology. The UAF Campus emitted 7.4 tons of SO<sub>2</sub> emissions in 2023 and is 117 kilometers from Denali National Park.
- Based on the information provided above, DEC has removed the UAF Campus from DEC's list of sources requiring further analysis as described in more detail in Section 2 of the enclosed document entitled, "2025 Review of Alaska's Potential Controllable Sources."

Regarding Golden Valley Electric Association's (GVEA) North Pole Power Plant:

- DEC evaluated firing ultra-low sulfur diesel (ULSD) year-round in EUs 1 and 2 at this facility as part of the SO<sub>2</sub> BACT analysis in the 2024 FNSB NAA PM<sub>2.5</sub> SIP Submission. DEC estimated that for ULSD, the SO<sub>2</sub> removal cost for EUs 1 and 2 would be between \$6,629 and \$13,932/ton based on potential to emit and between \$6,723 and \$14,026/ton

based on potential to emit, respectively (depending on fuel price). The documentation for this determination can be found on Regulations.gov for docket no. EPA-R10-OAR-2024-0595 here: <https://www.regulations.gov/document/EPA-R10-OAR-2024-0595-0078>

- DEC obtained updated fuel costs for the various fuel types provided to GVEA from Petro Star, Inc. These updated fuel prices included a change in the price difference between No. 1 and No. 2 fuel oil that means No. 1 fuel oil is not cost effective for EUs 1 and 2. Therefore, the North Pole Power Plant will no longer have a requirement to switch to No. 1 fuel oil on EUs 1 and 2. The updated analysis is enclosed in Section 3a of the enclosed document, “2025 Review of Alaska’s Potential Controllable Sources.”
- DEC has determined that firing ULSD in EUs 1 and 2 would not be cost-effective based on actual emissions for purposes of the regional haze long-term strategy.
- DEC evaluated requiring ULSD year-round in EUs 5 and 6 at this facility as part of the SO<sub>2</sub> BACT analyses in the FNSB NAA PM<sub>2.5</sub> SIP submitted on December 4, 2024. DEC estimated that for ULSD, the SO<sub>2</sub> removal cost for EUs 5 and 6 would be over \$2.5 million per ton of SO<sub>2</sub> removed based on potential to emit. Both units currently fire light-straight run (LSR), or naphtha, an inherently low sulfur fuel. The documentation for this determination can be found on Regulations.gov for docket no. EPA-R10-OAR- 2024-0595 at <https://www.regulations.gov/document/EPA-R10-OAR-2024-0595-0078>.
- DEC has determined that firing ULSD in EUs 5 and 6 would not be cost-effective based on actual emissions for purposes of the regional haze long-term strategy.
- Based on the information provided above, DEC has determined that it is economically infeasible to switch to ULSD for EUs 1, 2, 5, and 6 or to No. 1 fuel oil for EUs 1 and 2 at the North Pole Power Plant. Therefore, no reductions or emission controls were selected for North Pole Power Plant under the Regional Haze rule.

Regarding Golden Valley Electric Association’s (GVEA’s) Healy Power Plant:

- In the 2022 Regional Haze Plan SIP Submission, DEC completed a four-factor analysis on EU 1 because it was probable that the EU would be retiring. Based on the comprehensive best available retrofit technology (BART) analysis during the first implementation period, DEC determined that additional controls outside of DSI would not be cost effective. Therefore, to ensure SO<sub>2</sub> controls were fully evaluated, DEC articulated three options from EU 1: (1) retire Unit 1 by 2024, (2) submit a four-factor analysis for dry sorbent injection (DSI) optimization, or (3) accept a 0.20 lb/MMBtu SO<sub>2</sub> limit.
- After the 2022 Regional Haze Plan SIP Submission, GVEA elected to install SCR on EU 1 and continue operating the unit.
- GVEA submitted a four-factor analysis for optimizing DSI on June 30, 2023, with the conclusion that their DSI system could not achieve an SO<sub>2</sub> emissions rate lower than EU 1’s current emissions limit of 0.30 lb/MMBtu through increased sorbent injection rates alone.
- DEC also reevaluated whether DSI optimization is necessary for reasonable progress based on the four statutory factors. Additional details of DEC’s supplemental evaluation are in Section 3b of the enclosed document entitled “2025 Review of Alaska’s Potential Controllable Sources.” Based on this reevaluation which used DSI cost estimates from sources in the FNSB Serious NAA PM<sub>2.5</sub> SIP, DEC has determined that it is cost ineffective

to upgrade the DSI control system on the Healy Power Plant EU1. This analysis confirms the conclusion from the previous BART analysis.

- As stated in the 2022 Regional Haze Plan SIP Submission, further SO<sub>2</sub> control technology retrofits on EU 1 are not necessary for reasonable progress and EU 1 remains effectively controlled based on the existing 0.30 lb/MMBtu SO<sub>2</sub> limit embodied in a 2012 federal consent decree and approved by the EPA as BART.
- On April 8, 2025, GVEA Healy EU 1 received a Presidential Exemption from MATS compliance until July 2029. It is reasonable to assume that GVEA would time any upgrade to the DSI system to coincide with work to install activated carbon injection ports for MATS compliance.
- In the Regional Haze SIP for the second implementation period, DEC determined that the 54-MW TRW Integrated Entrained Combustion System (EU 2) at GVEA's Healy Power Plant is effectively controlled, with the unit's existing SO<sub>2</sub> emissions rate of 0.10 lb/MMBtu achieved using a Spray Dry Absorber control system. This requirement is embodied in a 2012 federal consent decree.

Regarding Aurora Energy's Chena Power Plant:

- DEC evaluated retrofitting EUs 4 through 7 at this facility with SO<sub>2</sub> emissions controls as part of the SO<sub>2</sub> BACT analyses in the FNSB NAA PM<sub>2.5</sub> SIP submitted on December 4, 2024. DEC determined that due to space constraints, it would not be technically feasible to install wet flue gas desulfurization (WFGD), circulating dry scrubbers (CDS), or SDA on EUs 4 through 7. Additionally, DEC determined that for DSI, the SO<sub>2</sub> removal cost would be \$13,368/ton based on potential to emit. The documentation for this determination can be found on Regulations.gov for docket no. EPA-R10-OAR-2024-0595 at <https://www.regulations.gov/document/EPA-R10-OAR-2024-0595-0078>.
- SO<sub>2</sub> emission limits were included in the power plant's operating permit under the FNSB NAA PM<sub>2.5</sub> SIP and included as regulatory required controls in the Second Implementation Regional Haze SIP. However, further studies determined that the controls did not meaningfully contribute to reducing PM<sub>2.5</sub> emissions in the Nonattainment Area. The documentation for this determination can be found in the Modeling Chapter for the FNSB NAA PM<sub>2.5</sub> SIP, available at <https://dec.alaska.gov/media/rs4pmcfa/iiid708-modeling.pdf>.
- DEC determined that retrofitting EUs 4 through 7 with a DSI system would not be cost effective based on actual SO<sub>2</sub> emissions for purposes of the Regional Haze long-term strategy.
- Based on the information provided above, DEC has determined that it is technically infeasible to install WFGD, CDS, or SDA based on space constraints, and it is not cost effective to install DSI on the coal-fired boilers at the Chena Power Plant. Therefore, no further emissions reductions or emissions controls are selected for the Chena Power Plant for the 2025 RH Clarifications Memo. Further analysis is described in more detail in Section 3c of the enclosed document entitled, "2025 Review of Alaska's Potential Controllable Sources."

Regarding Eielson Air Force Base (Eielson) Combined Heating and Power Plant:

- In 2010, DEC authorized a phased replacement of the base's six existing older coal-fired boilers without SO<sub>2</sub> controls with five new boilers that are designed to accommodate DSI systems to control SO<sub>2</sub> emissions. The sixth boiler was to be removed without a replacement. The first boiler was replaced in 2014 and a second in 2016. The other four original boilers remain onsite and continue to operate without SO<sub>2</sub> emission controls. With the boiler replacement project halted, DEC required the facility to do a Four Factor Analysis in 2023 for the installation of SO<sub>2</sub> pollution control technologies including WFGD, DSI, and SDA. Based on the results of this 2023 analysis, Eielson concluded that retrofitting the boilers with any SO<sub>2</sub> emission controls would be cost prohibitive.

DEC revised Eielson's analysis with conservative assumptions which also showed that retrofitting the older coal-fired boilers with new SO<sub>2</sub> emissions controls would be cost prohibitive for Regional Haze. Further analysis is described in more detail in Section 3d of the enclosed document entitled, "2025 Review of Alaska's Potential Controllable Sources."

- To further analyze the costs of retrofitting SO<sub>2</sub> controls on Eielson's four legacy coal-fired boilers EUs 1 through 4, DEC reviewed the SO<sub>2</sub> BACT analysis that was conducted as part of the 2024 FNSB NAA PM<sub>2.5</sub> SIP Submission, for the similar size and era EUs 1 through 6 at Fort Wainwright. As previously mentioned, DEC estimated that the lowest cost control option of DSI would cost \$6,636/ton of SO<sub>2</sub> removed based on potential to emit. However, this BACT analysis was based on the Fort Wainwright coal-fired boiler's combined potential emissions of 1,470 tons of SO<sub>2</sub>, which is substantially more than the 212 tons of combined SO<sub>2</sub> emissions emitted in 2023 from EUs 1 through 4 at Eielson that would be used in a four-factor analysis.

Therefore, DEC concludes that SO<sub>2</sub> controls would be cost prohibitive to install on Eielson's EUs 1 through 4 for the regional haze second implementation period. The documentation for this determination can be found on Regulations.gov for docket no. EPA-R10-OAR-2024-0595 at <https://www.regulations.gov/document/EPA-R10-OAR-2024-0595-0078>.

- In the 2022 Regional Haze Plan SIP Submission, DEC stated that Eielson's newer coal-fired boilers, EUs 5A and 6A, were already effectively controlled with DSI and an existing SO<sub>2</sub> emissions limit of 0.20 lb/MMBtu to comply with the performance standard for industrial-commercial-institutional steam generating units (NSPS Db). DEC further stated that SO<sub>2</sub> emissions from EUs 5A and 6A have been extremely low (5.9 tons in 2017, 22 tons in 2018, and 3.7 tons in 2019). Because this limit is embodied in a Federal NSPS standard and emissions from EUs 5A and 6A are documented in the submission as being extremely low, the existing limit is not necessary for reasonable progress in the regional haze second implementation period.



Regarding U.S. Army Garrison Fort Wainwright's Central Heating and Power Plant (CHPP):

- DEC evaluated retrofitting Units 1 through 6 at this facility with a DSI system as part of the SO<sub>2</sub> BACT analyses in the Fairbanks PM<sub>2.5</sub> SIP submitted on December 4, 2024. The Alaska DEC estimated that for DSI, the SO<sub>2</sub> removal cost would be \$6,636/ton based on potential to emit. DEC also determined the cost effectiveness of retrofitting Units 1 through 6 with CDS, WFGD, and SDA ranged from over \$13,000 per ton to over \$20,000 per ton of SO<sub>2</sub> removed based on potential to emit. The documentation for this determination can be found on Regulations.gov for docket no. EPA-R10-OAR-2024-0595 at <https://www.regulations.gov/document/EPA-R10-OAR-2024-0595-0078>.
- SO<sub>2</sub> emission limits were implemented in the facility's operating permit under the FNSB NAA PM<sub>2.5</sub> SIP and included as regulatory required controls in the Second Implementation Regional Haze SIP. However, further studies determined that the controls did not meaningfully contribute to reducing PM<sub>2.5</sub> emissions in the Nonattainment Area. The documentation for this finding can be found in the Modeling Chapter for the FNSB NAA PM<sub>2.5</sub> SIP, available at <https://dec.alaska.gov/media/rs4pmcfa/iid708-modeling.pdf>.
- DEC has determined that retrofitting EUs 1 through 6 with a DSI system would not be cost effective based on actual SO<sub>2</sub> emissions for purposes of the regional haze long-term strategy.
- Based on the information provided above, DEC has determined that it is economically infeasible to install CDS, WFGD, SDA, or DSI on the coal-fired boilers at the Fort Wainwright Power Plant. Therefore, no further emission reductions or emission controls were selected for EUs 1 through 6. Further analysis is described in Section 3e of the enclosed document entitled, "2025 Review of Alaska's Potential Controllable Sources."

As described above, analyses conducted on Alaska's anthropogenic sources indicated that the sources are effectively controlled or that additional emission controls would be economically infeasible. DEC further contends that visibility in each of Alaska's Class I areas is already achieving natural conditions.

However, many of the most significant impacts on Alaska's visibility are uncontrollable sources unique to the state and not properly accounted for in the modeling platforms available to DEC. Some of these impacts are illustrated in the results of a modeling effort conducted by EPA and described in the report entitled, "Technical Support Document for EPA's Updated 2028 Regional Haze Modeling for Hawaii, Virgin Islands, and Alaska." Modeling results demonstrated that even after accounting for international anthropogenic emissions and removing all U.S. anthropogenic sources, the forecasted 2028 Most Impaired Day annual average deciview value remained above the uniform rate of progress and the point almost identical to the unadjusted forecast at all four stations. This indicates that any visibility impairment above natural conditions is most likely due to uncontrollable natural sources. It also indicates that imposing additional emission restrictions on industrial sources such as the coal-fired boilers at the Golden Valley Electric Association Healy Power Plant or Eielson Air Force Base will not result in decreased visibility impairment at Denali National Park. DEC discusses this assertion in more detail in the enclosed document entitled "Alaska's Class I Area Visibility."

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Thank you for your time and attention to this matter. For any questions, please contact Director Jason Olds at [Jason.Olds@alaska.gov](mailto:Jason.Olds@alaska.gov).

Sincerely,



Randy Bates  
Commissioner

Enclosures: 2025 Review of Alaska's Potential Controllable Sources  
Alaska's Class I Area Visibility

cc: Jason Olds, Director, Air Quality

**Enclosure 1: 2025 Review of Alaska's Potential Controllable Sources**



## Enclosure 1: 2025 Review of Alaska’s Potential Controllable Sources

### 1. Overview/Purpose

40 CFR §51.308(f)(2)(i) of the Regional Haze (RH) Rule requires states to periodically revise and submit their State Implementation Plans (SIPs) to ensure continued improvement in visibility conditions at Class I federal areas. A state’s RH SIP submission must include a long-term strategy (LTS) that must “include emission limits, schedules of compliance and other measures as may be necessary to make reasonable progress” and “identify all anthropogenic sources of visibility impairment considered by the state in developing its long-term strategy”. In developing this LTS, the state selects sources for review (based on their impact on visibility conditions at Class I federal areas) and considers four factors for potential control measures for the selected sources: 1) cost of compliance; 2) time necessary to achieve compliance; 3) energy and non-air quality environmental impacts; and 4) remaining useful life. Consideration of visibility benefits is an optional fifth factor that states may consider per EPA’s August 2019 “Guidance on Regional Haze State Implementation Plans for the Second Implementation Period,” (2019 Guidance Document).

In support of the 2025 RH Clarifications Memo, the Alaska Department of Environmental Conservation (DEC) reviewed the updated actual emissions for the six stationary sources that were previously selected for review in the 2022 RH SIP. DEC reviewed the 2023 actual emissions as reported through the National Emissions Inventory (NEI) and performed an updated Q/d analysis, as outlined in Section 2 of this report. A list of the five sources selected for evaluation based on the updated Q/d analysis are shown in Table A.

**Table A - Facility Selection for Review**

| Facility               | Review Section |
|------------------------|----------------|
| North Pole Power Plant | 3.a            |
| Healy Power Plant      | 3.b            |
| Chena Power Plant      | 3.c            |
| Eielson Air Force Base | 3.d            |
| Fort Wainwright        | 3.e            |

## 2. Source Selection

To determine which stationary sources to carry forward for a four-factor analysis in the 2025 update, DEC reviewed the updated actual emissions from the sources that were previously selected in the 2022 RH SIP. These six sources were selected for review in the 2022 RH SIP using a Q/d analysis (i.e., actual SO<sub>2</sub> emissions from the source in 2017 (Q) / distance from the nearest Class I federal area (d)). If the Q/d ratio for a given source was calculated to be 1.0 or greater, then the source was selected for review in the 2022 RH SIP. For the 2025 updated source review, DEC reviewed the 2023 actual SO<sub>2</sub> emissions as reported through the NEI for these six stationary sources and performed an updated Q/d analysis. The updated Q/d analysis used the same 1.0 threshold used for the 2022 RH SIP to determine whether a source warranted further review.

The University of Alaska Fairbanks Campus (UAF Campus) had two coal-fired boilers EUs 1 and 2 in operation during the 2017 NEI year with 126.6 tons of SO<sub>2</sub> emissions combined. Those two EUs have since retired and been replaced by a new dual fuel-fired boiler EU 113, that primarily burns coal and is equipped with fluidized bed limestone injection controls. Consequently, the 2023 SO<sub>2</sub> NEI emissions reported for UAF Campus's emissions unit inventory were 7.4 tons. Based on the UAF Campus's reported actual SO<sub>2</sub> emissions of 7.4 tons for the year 2023 and the facility's distance from Denali National Park of 117 kilometers, the updated Q/d calculation for the UAF Campus results in a ratio of 0.1. A Q/d ratio of 0.1 is well below the 1.0 threshold set by DEC to determine whether a source warrants further review. Therefore, in this updated 2025 source review, the UAF Campus has been removed from DEC's list of sources that require further analysis.

Golden Valley Electric Association's (GVEA's) North Pole Power Plant (NPPP) had actual SO<sub>2</sub> emissions in 2023 of 38.9 tons, which resulted in a Q/d ratio of 0.32. However, in 2023 the NPPP had SO<sub>2</sub> fuel limits in place from the Fairbanks North Star Borough PM<sub>2.5</sub> Serious Nonattainment Area (FNSB NAA) SIP that have since been rescinded. Therefore, when calculating Q/d for the NPPP, the Department used 2024 actual emissions which were not impacted by the limits from FNSB NAA SIP. GVEA reported actual SO<sub>2</sub> emissions of 148 tons in 2024, which resulted in an updated Q/d ratio of 1.2. Therefore, DEC included the NPPP in the updated 2025 source review for further analysis which is discussed in more detail below.

After completing the source selection process as described above for the rest of the sources previously selected in the 2022 RH SIP (i.e., performing an updated Q/d analysis for each of the six sources), DEC has identified five sources that warrant further evaluation in this updated 2025 source review, which are listed below in Table B.

**Table B - 2025 Facility Selection for Review**

| Facility               | Nearest Monitor | Distance to Monitor d (km) | Quantity of SO <sub>2</sub> Emissions Q (tpy) | Q/d SO <sub>2</sub> | Section Number |
|------------------------|-----------------|----------------------------|---|---------------------|----------------|
| North Pole Power Plant | Denali N.P.     | 122                        | 148.0   | 1.2                 | 3.a            |
| Healy Power Plant      | Denali N.P.     | 6                          | 319.0   | 53.2                | 3.b            |

| Facility               | Nearest Monitor | Distance to Monitor d (km) | Quantity of SO <sub>2</sub> Emissions Q (tpy) | Q/d SO <sub>2</sub> | Section Number |
|------------------------|-----------------|----------------------------|---|---------------------|----------------|
| Chena Power Plant      | Denali N.P.     | 119                        | 228.6   | 1.9                 | 3.c            |
| Eielson Air Force Base | Denali N.P.     | 133                        | 233.7   | 1.8                 | 3.d            |
| Fort Wainwright        | Denali N.P.     | 119                        | 397.9   | 3.3                 | 3.e            |

### 3. Four-Factor Analysis

#### a. Golden Valley Electric Association, North Pole Power Plant (NPPP)

##### Introduction and 2022 RH SIP Findings

The NPPP is an electric generating facility owned and operated by GVEA that currently operates under Title V Operating Permit AQ0110TVP04 Rev. 1. The standard industrial classification (SIC) code for this stationary source is 4911 - Electric Services. The power plant contains two fuel oil-fired simple cycle gas combustion turbines, two fuel oil-fired combined cycle gas combustion turbines, one fuel oil-fired emergency generator, and two propane fired boilers. These EUs are listed below in Table C. The stationary source also owns insignificant EUs that include several gas-fired heaters.

**Table C - GVEA North Pole Power Plant Emissions Units**

| EU ID | Emissions Unit Name | Emissions Unit Description  | Fuel              | Rating/Size                   | Installation or Construction Date |
|-------|---------------------|---|-------------------|-------------------------------|-----------------------------------|
| 1     | GT#1                | GE Frame 7, Series 7001 Regenerative Gas Turbine  | Fuel Oil          | 672 MMBtu/hr (60.5 MW)        | 1976                              |
| 2     | GT#2                | GE Frame 7, Series 7001 Regenerative Gas Turbine  | Fuel Oil          | 672 MMBtu/hr (60.5 MW)        | 1977                              |
| 5     | GT#3                | GE LM6000PC Gas Turbine<br>(water injection for NO <sub>x</sub> control)<br>(oxidation catalyst for CO control) | Naphtha/LSR Jet A | 455 MMBtu/hr (43 MW, nominal) | 2005                              |
| 6     | GT#4                | GE LM6000PC Gas Turbine<br>(water injection for NO <sub>x</sub> control)<br>(oxidation catalyst for CO control) | Naphtha/LSR Jet A | 455 MMBtu/hr (43 MW, nominal) | Not Installed <sup>1</sup>        |
| 7     | Emergency Generator | Mitsubishi Engine #0A8829<br>(Generac Gen Set #5231150100)  | Fuel Oil          | 565 hp                        | 2005                              |
| 11    | Building Boiler     | Bryan Steam RV500 Boiler  | Propane           | 5.0 MMBtu/hr                  | 2005                              |
| 12    | Building Boiler     | Bryan Steam RV500 Boiler  | Propane           | 5.0 MMBtu/hr                  | 2005                              |

Table Note: <sup>1</sup> Estimated installation is 2024.

For the 2022 RH SIP analysis for the NPPP, DEC partially relied upon findings contained in the FNSB NAA SIP that required fuel switches for the turbines contained at the stationary source. However, the SO<sub>2</sub> BACT requirements contained in the 2019/2020 FNSB NAA SIP were

withdrawn by DEC on September 25, 2023. An updated BACT analysis was included with the submittal of the 2024 FNSB SIP Amendment,<sup>1</sup> which contained a major source precursor demonstration for SO<sub>2</sub> emissions. Therefore, DEC has performed a new four factor analyses for SO<sub>2</sub> emissions on the turbines.

In the 2022 RH SIP, DEC compiled a list of SO<sub>2</sub> emissions at the stationary source using the NEI submissions for years 2014-2019 which can be seen in Table D. As can be seen in Table D, EUs 1, 2, and 5 are the only EUs with sizeable SO<sub>2</sub> emissions over the past 6 years. Therefore, DEC chose to perform a four-factor analysis of the NPPP on EUs 1, 2, and 5. This decision to analyze EUs 1, 2, and 5 has been carried forward into the updated 2025 source review as the back-up generator, EU 7, and the 5 MMBtu/hr propane-fired boilers, EUs 11 and 12, continue to emit negligible amounts of SO<sub>2</sub> emissions.

**Table D - North Pole Power Plant SO<sub>2</sub> Emissions**

| <b>Calendar Year</b> | <b>EU ID</b> | <b>SO<sub>2</sub> Emitted (tons) Emissions Inventory</b> | <b>SO<sub>2</sub> Emitted (tons) Emissions Inventory</b> |
|----------------------|--------------|--|--|
| 2019                 | 1            | 17.04  | 268.4  |
|                      | 2            | 251.03   |  |
|                      | 5            | 0.32   |  |
|                      | 7            | 0.00   |  |
|                      | 11           | 0.00   |  |
|                      | 12           | 0.00   |  |
| 2018                 | 1            | 19.8   | 215.2  |
|                      | 2            | 189.84   |  |
|                      | 5            | 5.58   |  |
|                      | 7            | 0.00   |  |
|                      | 11           | 0.00   |  |
|                      | 12           | 0.00   |  |
| 2017                 | 1            | 31.68  | 269.5  |
|                      | 2            | 228.87   |  |
|                      | 5            | 8.89   |  |
|                      | 7            | 0.00   |  |
|                      | 11           | 0.00   |  |
|                      | 12           | 0.00   |  |
|                      | 1            | 37.87  |  |
|                      | 2            | 190.76   |  |

<sup>1</sup> DEC's 2024 FNSB NAA SIP Amendment: <https://dec.alaska.gov/air/anpms/communities/fbks-pm2-5-2024-amendment-serious-sip/>.

| Calendar Year | EU ID | SO <sub>2</sub> Emitted (tons) Emissions Inventory | SO <sub>2</sub> Emitted (tons) Emissions Inventory |
|---------------|-------|--|--|
| 2016          | 5     | 11.20  | 239.8  |
|               | 7     | 0.00   |  |
|               | 11    | 0.00   |  |
|               | 12    | 0.00   |  |
| 2015          | 1     | 8.47   | 149.1  |
|               | 2     | 131.74   |  |
|               | 5     | 8.84   |  |
|               | 7     | 0.00   |  |
|               | 11    | 0.00   |  |
|               | 12    | 0.00   |  |
| 2014          | 1     | 5.64   | 148.4  |
|               | 2     | 138.15   |  |
|               | 5     | 4.58   |  |
|               | 7     | 0.00   |  |
|               | 11    | 0.00   |  |
|               | 12    | 0.00   |  |

### 2022 DEC Regional Haze Findings for GVEA's North Pole Power Plant

After performing four-factor analyses for switching the turbines, EUs 1 and 2, to ULSD and No. 1 fuel oil, and EU 5 to ULSD, DEC found that it was cost-effective and feasible for GVEA to switch EUs 1 and 2 to fuel oil with a maximum sulfur content of 0.1 percent by weight (1,000 ppmw, No. 1 fuel oil). This finding was predicated on the assumption that GVEA would be able to purchase No. 1 fuel oil from the Petro Star North Pole Refinery (PSNPR). If the PSNPR was not able to supply GVEA with No. 1 fuel oil due to shortages in supply, the NPPP could continue to burn No. 2 fuel oil in EUs 1 and 2 until such time as No. 1 fuel oil is again available to GVEA's NPPP. A summary of DEC's 2022 RH SIP findings is listed below:

**Table E - 2022 RH SIP Final Determination for GVEA – North Pole Power Plant**

| Pollutant   | Regional Haze Controls   | Regional Haze Determination   | Effective Dates of Control/Limit  |
|---|--|---|---|
| <b>EUs 1 and 2 – Fuel Oil-Fired Simple Cycle Gas Turbines - 672 MMBtu/hr (each)</b> |  |   |   |
| SO <sub>2</sub>   | Clean Fuel Switch to No. 1 fuel oil  | Switch to fuel oil with a maximum sulfur content of 0.1 percent by weight (1,000 ppmw, No. 1 Fuel Oil)* | Submit permit application by January 1, 2024<br><br>Expect permit issuance by January 1, 2025 |
| <b>EUs 5 and 6 – Combined Cycle Gas Turbines - 455 MMBtu/hr (each)</b>              |  |   |   |
| SO <sub>2</sub>   | Already Effectively Controlled<br>(50 ppmw sulfur limit in fuel except during startup) | No Additional Control   | N/A   |

\* This finding is predicated on the assumption that GVEA will be able to purchase No. 1 fuel oil from the Petro Star North Pole Refinery. If the North Pole Refinery is not able to supply GVEA with No. 1 fuel oil due to shortages in supply, the NPPP may continue to burn No. 2 fuel oil in EUs 1 and 2 until such time as No. 1 fuel oil is again available.

### 2025 Updated RH SO<sub>2</sub> Four-Factor Analysis

Section 169A(g)(1) of the CAA lists four factors that must be taken into consideration in determining reasonable progress and states are required to consider those four factors (i.e., cost of compliance, time necessary for compliance, energy and non-air environmental impacts, and remaining useful life of the source) in the control analysis step.

### Cost of Compliance for the Fuel Oil-Fired Simple Cycle Gas Turbines (EUs 1 and 2)

The cost of compliance estimates the values of capital costs, annual operating and maintenance costs, annualized costs, and cost per ton of emission reductions that have been prepared according to EPA's Air Pollution Control Cost Manual. Costs are expressed in terms of cost effectiveness in the standardized unit of dollars per ton of actual SO<sub>2</sub> emissions reduced. DEC used information from the BACT analyses completed for the Fairbanks Serious SIP for SO<sub>2</sub> to complete the cost of compliance analyses. This information included previous BACT determinations found in the RACT, BACT, & LAER Clearinghouse (RBLC) database; internet research; and BACT analyses submitted to DEC by GVEA for the NPPP and Zehnder Facility.

The RBLC was searched for all determinations in the last 10 years under the process code 15.190 for simple cycle gas turbines (rated at 25 MW or more) The search results for simple cycle gas turbines are summarized in Table F.

**Table F - RBLC Summary of SO<sub>2</sub> Controls for Fuel Oil-Fired Simple Cycle Gas Turbines**

| Control Technology                | Number of Determinations | Emission Limits |            |
|-----------------------------------|--------------------------|-----------------|------------|
| Ultra-Low Sulfur Diesel           | 7                        | 0.0015          | % S by wt. |
| Fuel Oil (0.1 % S by wt. or less) | 2                        | 0.0026 – 0.055  | lb/MMBtu   |
| Good Combustion Practices         | 3                        | 0.6             | lb/hr      |



## **RBLC Review**

A review of similar units in the RBLC indicates that limiting the sulfur content of fuel and good combustion practices are the principle SO<sub>2</sub> control technologies determined as BACT for fuel oil-fired simple cycle gas turbines. The lowest SO<sub>2</sub> emission rate listed in the RBLC is combustion of ULSD at 0.0015 percent sulfur by weight (% S by wt.).

## **Identification of SO<sub>2</sub> Control Technology for the Simple Cycle Gas Turbines**

From research, DEC identified the following technologies as available for control of SO<sub>2</sub> emissions from fuel oil-fired simple cycle gas turbines rated at 25 MW or greater:

### **Ultra Low Sulfur Diesel (ULSD)**

ULSD has a fuel sulfur content of 0.0015 % S by wt. or less. Combusting ULSD as the primary fuel would reduce SO<sub>2</sub> emissions because the fuel oil-fired simple cycle gas turbines have historically mostly combusted No. 2 fuel oil that has a sulfur content averaging around 0.3 % S by weight.<sup>2</sup> Switching to ULSD would result in around a 99.5 percent decrease in SO<sub>2</sub> emissions from the fuel oil-fired simple cycle gas turbines. DEC considers ULSD a technically feasible control technology for the fuel oil-fired simple cycle gas turbines.

### **No. 1 Fuel Oil (maximum sulfur content of 0.1 % S by wt.)**

The No. 1 fuel oil available from the PSNPR comes in two different grades, a high sulfur version (HSHO#1) with a sulfur content of < 0.14 % S by wt. (1,400 ppmw) and a low sulfur version (LSHO#1) with a sulfur content of < 0.10 % S by wt. (1,000 ppmw). Combusting fuel with a sulfur content of 0.10 % to 0.14 % S by wt. as the primary fuel would reduce SO<sub>2</sub> emissions because the fuel oil-fired simple cycle gas turbines mostly combust No. 2 fuel oil that has a sulfur content of around 0.30 % S by weight. Switching to No. 1 fuel oil would result in an approximate 56% to 69% percent decrease in SO<sub>2</sub> emissions from the fuel oil-fired simple cycle gas turbines. DEC considers low sulfur diesel a technically feasible control technology for the fuel oil-fired simple cycle gas turbines. However, the 2024 Amendment to the FNSB NAA SIP<sup>3</sup> required that heating oil sold inside the NAA had to meet the requirements of LSHO#1 for all sources except for the major stationary sources that went through the BACT process. Consequently, there is greater demand for LSHO#1, which has caused a shortage of LSHO#1 in the Fairbanks area or the NAA. Thus, PSNSR is not providing LSHO#1 to GVEA at this time. Therefore, HSHO#1 is the only type of No. 1 fuel oil available to GVEA.

## **Eliminate Technically Infeasible SO<sub>2</sub> Technologies for the Simple Cycle Gas Turbines**

All control technologies identified are technically feasible for the fuel oil-fired simple cycle gas turbines.

## **Rank the Remaining SO<sub>2</sub> Control Technologies for the Simple Cycle Gas Turbines**

The following control technologies have been identified and ranked for control of SO<sub>2</sub> from the fuel oil-fired simple cycle gas turbines (Table G):

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<sup>2</sup> Note that the 0.3% S by weight value for No. 2 fuel oil is from the 2022 NEI. The source did not combust No. 2 fuel oil in 2023 due to SO<sub>2</sub> BACT limits from the FNSB NAA SIP that have since been rescinded.

<sup>3</sup> DEC's 2024 FNSB NAA SIP Amendment: <https://dec.alaska.gov/air/anpms/communities/fbks-pm2-5-2024-amendment-serious-sip/>.

**Table G - Control Technologies**

| <b>Control Technology</b> | <b>Control Level</b> |
|---------------------------|----------------------|
| Ultra Low Sulfur Diesel   | 99.5% Control        |
| No. 1 Fuel Oil            | 57% - 69.3% Control  |

Table Note: Control technologies already required at the stationary source, including practicing good combustion practices, or those included in the design of the EU are considered 0% control for the purposes of this four-factor analysis.

### **Evaluate the Most Effective Controls**

GVEA provided an economic analysis for the FNSB NAA SIP BACT exercise for switching the fuel combusted in the simple cycle gas turbines to No. 1 fuel oil and ULSD. For the updated 2025 source review, DEC updated GVEA's cost analysis with new data provided by PSNPR on August 14, 2025, for the cost per gallon of ULSD, HSHO#1, and No. 2 fuel oils delivered to the NPPP from January through July of 2025.

### **Department Cost Analysis for SO<sub>2</sub> Emissions Controls from the Simple Cycle Gas Turbines**

PSNPR sits adjacent to the NPPP and is the exclusive fuel supplier for the facility. Because the FNSB NAA SIP required all sales of heating oil in the NAA to be LSHO#1, there is not enough supply for the turbines at the NPPP. Therefore, DEC's updated cost analyses for EUs 1 and 2 calculated a cost per ton of SO<sub>2</sub> emissions removed resulting from a switch to ULSD and HSHO#1. There is no capital cost involved with this fuel switch for these EUs. Therefore, the only value driving cost for the evaluation was the yearly cost difference in fuel prices between No. 2 fuel oil compared to ULSD and HSHO#1. From January through July 2025, the average price per gallon of ULSD delivered to the NPPP was \$2.93. This price represents an increase of \$0.65 more per gallon of fuel if the facility were to switch from No. 2 fuel oil which has a cost of \$2.28 per gallon. During this same period, the average price per gallon for No. 1 fuel oil (HSHO#1) was \$2.57, which is \$0.29 more per gallon than the cost of No. 2 fuel oil at \$2.28 per gallon. For the cost analysis, the Department used a conservative approach which included the total amount of fuel combusted by EUs 1 and 2 in the 2023 NEI. However, because the FNSB NAA SIP limits were in effect at the time, all the fuel that was combusted in the turbines in 2023 was No. 1 fuel oil and ULSD. Now that those BACT limits have been withdrawn, the NPPP has continued to combust No. 2 fuel oil as their primary fuel source. However, note that the only factor driving the cost effectiveness value is the price per gallon of fuel. Therefore, the cost effectiveness value is not affected by the total amount of gallons purchased, as the reduction in emissions is directly proportional to the amount of fuel purchased.

A summary of these analyses is shown in Table H and Table I.

**Table H - DEC Economic Analysis for Technically Feasible SO<sub>2</sub> Controls for EU 1**

| Control Alternative  | 2023 SO <sub>2</sub> Emissions (tons) <sup>4</sup> | Emission Reduction (tpy) | Total Capital Investment (\$) | Total Annualized Costs (\$/year) | Cost Effectiveness (\$/ton) |
|--|--|--------------------------|-------------------------------|----------------------------------|-----------------------------|
| ULSD   | 9.82   | 9.77                     | N/A                           | \$289,614                        | \$29,646                    |
| No. 1 Fuel Oil (HSHO#1)  | 9.82   | 5.59                     | N/A                           | \$129,234\$                      | \$23,110                    |
| Capital Recovery Factor = 0.0 (There is no capital investment involved with this cost calculation) |  |                          |                               |                                  |                             |

**Table I - DEC Economic Analysis for Technically Feasible SO<sub>2</sub> Controls for EU 2**

| Control Alternative  | 2023 SO <sub>2</sub> Emissions (tons) <sup>5</sup> | Emission Reduction (tpy) | Total Capital Investment (\$) | Total Annualized Costs (\$/year) | Cost Effectiveness (\$/ton) |
|--|--|--------------------------|-------------------------------|----------------------------------|-----------------------------|
| ULSD   | 182.18   | 181.27                   | N/A                           | \$5,374,048                      | \$29,646                    |
| No. 1 Fuel Oil (HSHO#1)  | 182.18   | 103.77                   | N/A                           | \$2,398,063                      | \$23,110                    |
| Capital Recovery Factor = 0.0 (There is no capital investment involved with this cost calculation) |  |                          |                               |                                  |                             |

DEC's cost of compliance economic analysis indicates the level of SO<sub>2</sub> reduction does not justify the use of ULSD or HS#1 fuel oil for the fuel oil-fired simple cycle gas turbines at the NPPP with a cost of \$29,646/ton and \$23,110/ton respectively. Because the economic analysis showed a fuel switch to be cost ineffective, DEC did not evaluate the other three factors included in the four-factor analysis. Therefore, there is no emission limit or control selected for EUs 1 and 2 as a part of the RH four-factor analysis.

#### **Cost of Compliance for the Fuel Oil-Fired Combined Cycle Gas Turbine (EU 5)**

The cost of compliance estimates the values of capital costs, annual operating and maintenance costs, annualized costs, and cost per ton of emission reductions that have been prepared according to EPA's Air Pollution Control Cost Manual. Costs are expressed in terms of cost effectiveness in the standardized unit of dollars per ton of actual SO<sub>2</sub> emissions reduced. DEC used information from the BACT analyses completed for the Fairbanks Serious SIP for SO<sub>2</sub> to complete the cost of compliance analyses. This information included previous BACT determinations found in the RBLC database, internet research, and BACT analyses submitted to DEC by GVEA for the NPPP and Zehnder Facility.

<sup>4</sup> Note that this value is not the actual 2023 emissions for EUs 1 and 2, instead it is a conservative estimate of what the actual emissions for 2023 would have been if the source combusted No. 2 fuel oil exclusively instead of No. 1 fuel oil and ULSD. GVEA reported SO<sub>2</sub> emissions of 1.91 tons for EU 1 and 33.30 tons for EU 2 in the 2023 NEI.

<sup>5</sup> See Footnote 4.

The RBLC was searched for all determinations in the last 10 years under the process code 15.290 for combined cycle gas turbines (rated at 25 MW or more) The search results for combined cycle gas turbines are summarized in Table J.

**Table J - RBLC Summary of SO<sub>2</sub> Controls for Fuel Oil-Fired Combined Cycle Gas Turbines**

| Control Technology      | Number of Determinations | Emission Limits |
|-------------------------|--------------------------|-----------------|
| Ultra-Low Sulfur Diesel | 1                        | 0.15 by wt.     |

#### **RBLC Review**

A review of similar units in the RBLC indicates that limiting the sulfur content of fuel is the principle SO<sub>2</sub> control technologies determined as BACT for fuel oil-fired combined cycle gas turbines. The lone SO<sub>2</sub> limit listed in the RBLC is for combustion of ULSD.

#### **Identification of SO<sub>2</sub> Control Technology for the Fuel Oil-fired Combined Cycle Gas Turbines**

From research, DEC identified the following technologies as available for controlling SO<sub>2</sub> emissions from fuel oil-fired combined cycle gas turbines rated at 25 MW or greater:

##### **Ultra Low Sulfur Diesel (ULSD)**

The methods by which combusting ULSD reduces sulfur emissions were discussed in detail in above in the section titled “Identification of SO<sub>2</sub> Control Technology for the Fuel Oil-Fired Simple Cycle Turbines,” and will not be repeated here. DEC considers ULSD a technically feasible control technology for the fuel oil-fired combined cycle gas turbines.

##### **Light Straight Run Turbine Fuel (LSR)**

EU 5 typically combusts LSR when not in startup, which had an average concentration of 0.0023 % S by wt. as reported by GVEA in their 2023 NEI. DEC considers operating LSR a technically feasible control technology for the fuel oil-fired combined cycle gas turbines.

##### **Eliminate Technically Infeasible SO<sub>2</sub> Technologies for the Combined Cycle Gas Turbines**

All control technologies identified are technically feasible for the fuel oil-fired combined cycle gas turbines.

##### **Rank point the Remaining SO<sub>2</sub> Control Technologies for the Combined Cycle Gas Turbines**

The following control technology has been identified and ranked for control of SO<sub>2</sub> from the fuel oil-fired combined cycle gas turbines (Table K).

**Table K - Control Technology**

| Control Technology      | Control Level |
|-------------------------|---------------|
| Ultra Low Sulfur Diesel | 77.2% Control |

Table Note: Control technologies already required at the stationary source, including burning LSR except during startup and practicing good combustion practices, or those included in the design of the EU are considered 0% control for the purposes of this four-factor analysis.

### Evaluate the Most Effective Controls

GVEA provided an economic analysis for the Serious SIP BACT exercise for switching the fuel combusted in the combined cycle gas turbine to ULSD. DEC used this cost analysis and an update provided by GVEA for the cost per gallon of No. 1 fuel oil, ULSD and LSR delivered to the NPPP between January 2019 and October 2020 to perform our cost analysis.

### Department Evaluation of BACT for SO<sub>2</sub> Emissions from the Combined Cycle Gas Turbines

DEC's cost analysis calculated the cost per ton of SO<sub>2</sub> emissions removed resulting from a switch to ULSD. There is no capital cost involved with this fuel switch for EU 5. Therefore, the only value driving cost for the evaluation was the yearly cost difference in fuel prices between LSR and No. 1 (used during start-up) compared to ULSD.

A summary of these analyses is shown in Table L.

**Table L - Department Economic Analysis for Technically Feasible SO<sub>2</sub> Controls for EU 5**

| Control Alternative  | 2016 SO <sub>2</sub> Emissions (tons) | Emission Reduction (tpy) | Total Capital Investment (\$) | Total Annualized Costs (\$/year) | Cost Effectiveness (\$/ton) |
|--|---------------------------------------|--------------------------|-------------------------------|----------------------------------|-----------------------------|
| ULSD   | 10.75                                 | 8.30                     | N/A                           | \$12,802,923                     | \$1,542,463                 |
| Capital Recovery Factor = 0.0 (There is no capital investment involved with this cost calculation) |                                       |                          |                               |                                  |                             |

DEC's cost of compliance economic analysis indicates the level of SO<sub>2</sub> reduction does not justify the use of ULSD for the fuel oil-fired combined cycle gas turbine at the NPPP (\$1,542,463/ton). Because the economic analysis showed a fuel switch to be cost ineffective, DEC did not evaluate the other three factors included in the four-factor analysis. Therefore, there is no emission limit or control selected for EU 5 as a part of the RH four-factor analysis. DEC notes that this analysis was based on actual emissions and therefore only EU 5 was evaluated. However, the Permittee is authorized to install an identical fuel oil-fired combined cycle gas turbine (EU 6) under prior air quality permitting. Therefore, this evaluation for EU 5 is also considered an evaluation for EU 6 upon installation.

### DEC 2025 Regional Haze Findings for North Power Plant

DEC finds that it is economically infeasible to switch to ULSD for EUs 1, 2, 5, and 6, or HS#1 fuel oil for EUs 1 and 2 at the North Pole Power Plant. Therefore, no further emissions reductions or emissions controls are selected for the North Pole Power Plant.

**b. Golden Valley Electric Association: Healy Power Plant**

**Introduction and 2022 RH SIP Findings**

The Healy Power Plant is an electric generating facility owned and operated by GVEA, and GVEA is the Permittee for the stationary source's Title V Operating Permit AQ0173TVP03. The SIC code for this stationary source is 4911 – Electrical Power Generation. The primary power generating units include two coal-fired steam generators: the 25-MW Foster-Wheeler Unit No. 1 (EU 1) and the 54-MW TRW Integrated Entrained Combustion System (EU 2) formerly known as the Healy Clean Coal Project (HCCP). The stationary source also operates two Cleaver Brooks standby building boilers (EUs 3 and 4), one standby diesel generator (EU 5), and a firewater pump engine (EU 13). These emissions units (EUs) are listed below in Table M.

**Table M - Healy Power Plant Emission Unit Inventory**

| <b>EU ID</b> | <b>Emissions Unit Name</b>         | <b>Emissions Unit Description</b>   | <b>Rating/Size</b> | <b>Construction Date</b> |
|--------------|------------------------------------|---|--------------------|--------------------------|
| 1            | Unit No. 1                         | Foster-Wheeler Boiler, pulverized coal fired steam generator with a 12 module ICA baghouse, SN 78-266   | 327 MMBtu/hr       | November 1967            |
| 2            | Unit No. 2                         | TRW Integrated Entrained Combustion System, pulverized coal-fired steam generator with Joy activated recycle spray dryer absorber and Joy pulse jet fabric filter, SN 1 | 658 MMBtu/hr       | 1996                     |
| 3            | Auxiliary Boiler No. 1             | Cleaver Brooks CB 189-300, Standby process and building boiler, SN L-39759, Diesel-fired  | 12.554 MMBtu/hr    | 1967                     |
| 4            | Auxiliary Boiler No. 2             | Cleaver Brooks CB 100-800-15, Standby process and building boiler, SN OLO94777, Diesel-fired  | 23.0 MMBtu/hr      | 1996                     |
| 5            | Diesel Generator No. 1             | Electro-Motive Diesel, EMD 20-645-E4, SN 67-B1-1152 (engine)<br>Standby diesel generator, SN A-20-D (generator)   | 2.75 MW            | 1967                     |
| 6            | Crusher System                     | Crusher System2<br>SN 885247 (Secondary Crusher No. 1)<br>SN 844034 (Secondary Crusher No. 2)   | 12,000 cfm         | 1996                     |
| 73           | Limestone Storage Silo             | Limestone Storage Silo with baghouse  | 800 cfm            | 1996                     |
| 8            | Flyash Storage Silo                | Flyash Storage Silo with baghouse   | 5,000 cfm          | 1996                     |
| 9            | Sodium Bicarbonate Handling System | Sodium bicarbonate handling system4   | 440 cfm            | 1998                     |

| EU ID                            | Emissions Unit Name                      | Emissions Unit Description  | Rating/Size   | Construction Date |
|----------------------------------|--|---|---|-------------------|
| 10                               | Coal Handling System (dust collector #2) | Coal Handling System5   | 20,000 cfm  | 1996              |
| 13                               | Firewater Pump Engine                    | Caterpillar Diesel Model 3406B, Diesel-fired firewater pump engine; SN 6TB14931         | 264 hp  | 1997              |
| <b>Fugitive Emission Sources</b> |  |   |   |                   |
| 11                               | Haul Road                                | Haul Road (located on GVEA property) from Usibelli Coal Mine property line to coal pile | 0.25 miles  | 1967              |
| 12                               | Coal Storage Pile                        | Open Coal Storage Piles   | Up to 15-day coal supply, with both EU IDs 1 and 2 in operation | 1967              |

For the 2022 RH SIP, DEC performed a limited review in place of a full four-factor analysis because the stationary source already had dry sorbent injection (DSI) emissions controls installed on EU 1 and spray dry absorber (SDA) emissions controls installed on EU 2. Additionally, GVEA is under a Consent Decree (CD) with the EPA which required GVEA to decide on or before December 31, 2022, to either install SCR (or an alternative NO<sub>x</sub> control technology approved by EPA) on EU 1 or to retire the boiler. The deadline to have SCR installed on EU 1 or to have the EU retired was no later than December 31, 2024. Note that since the 2022 RH SIP, GVEA has decided to not retire EU 1, and has since installed and began operating an SCR unit on EU 1. DEC reviewed the previous six-year period (2014-2019) for which data was currently available to determine the source's SO<sub>2</sub> emissions. Table N shows SO<sub>2</sub> emissions reported to DEC through the NEI for 2014 and 2016 through 2019 (the years that NEI information was available for the source) and used the emissions fee estimate for 2015.

**Table N - Healy Power Plant SO<sub>2</sub> Emissions**

| Calendar Year | Coal-Fired Boilers SO <sub>2</sub> Emitted (tons) | Other EUs SO <sub>2</sub> Emitted (tons) | Total SO <sub>2</sub> Emitted (tons) |
|---------------|---|--|--------------------------------------|
| 2019          | 318.09  | 0.00                                     | 318.09                               |
| 2018          | 376.02  | 0.00                                     | 376.02                               |
| 2017          | 296.40  | 0.00                                     | 296.40                               |
| 2016          | 427.20  | 0.00                                     | 427.20                               |
| 2015          | 689.00  | 0.00                                     | 689.00                               |
| 2014          | 444.94  | 0.00                                     | 444.94                               |



As can be seen from Table N, the SO<sub>2</sub> emissions emitted at the Healy Power Plant are from the two coal-fired boilers EUs 1 and 2. Consequently, EUs 1 and 2 were the primary focus during the 2022 RH SIP, which treated SO<sub>2</sub> as the primary pollutant of concern. Condition 44 of Operating Permit AQ0173TVP03 limits EU 2 to an SO<sub>2</sub> emissions rate of no more than 0.10 lb/MMBtu, and Condition 44.1 requires EU 2 to use SDA when in operation. Condition 45 of Operating Permit AQ0173TVP03 limits EU 1 to an SO<sub>2</sub> emissions rate of no more than 0.30 lb/MMBtu, and Condition 45.1 requires EU 1 to use DSI when in operation. Section II.B.3.f. of the 2019 Guidance Document discusses selecting sources that already have effective emission control technology in place. The 2019 Guidance Document states the following:

“It may be reasonable for a state not to select an effectively controlled source. A source may already have effective controls in place as a result of a previous RH SIP or to meet another CAA requirement. In general, if post-combustion controls were selected and installed recently (see illustrative examples below) to meet a CAA requirement, there will be only a low likelihood of a significant technological advancement that could provide further reasonable emission reductions having been made in the intervening period. If a source owner has recently made a significant expenditure that has resulted in significant reductions of visibility impairing pollutants at an emissions unit, it may be reasonable for the state to assume that additional controls for that unit are unlikely to be reasonable for the upcoming implementation period. A state that does not select a source or sources for the following or any similar reasons should explain why the decision is consistent with the requirement to make reasonable progress, i.e., why it is reasonable to assume for the purposes of efficiency and prioritization that a full four-factor analysis would likely result in the conclusion that no further controls are necessary.”

In addition, Section II.B.3.f. of the 2019 Guidance Document also goes on to state:

“BART-eligible units that installed and began operating controls to meet BART emission limits for the first implementation period, on a pollutant-specific basis. Although the Regional Haze Rule anticipates the re-assessment of BART-eligible sources under the reasonable progress Rule provisions, if a source installed and is currently operating controls to meet BART emission limits, it may be unlikely that there will be further available reasonable controls for such sources. However, states may not categorically exclude all BART-eligible sources, or all sources that installed BART controls, as candidates for selection for analysis of control measures.”

Additionally, Section II.B.3.d. of the 2019 Guidance Document discusses the option to consider the four statutory factors when selecting sources and states the following:

“EPA expects that, typically, states are more likely to select sources based on visibility impacts and not consider the four reasonable progress factors (i.e., cost of compliance, remaining useful life, time necessary for compliance, and energy and non-air quality environmental impacts) until after a source is selected. However, in some cases, a state may already have information on one or more of the four reasonable progress factors at the time of source selection. If so, the state may consider that information at the source-selection stage. In particular circumstances, that information may indicate that it is reasonable to exclude the source for evaluation of emission control measures because it is clear at this step that no additional control measures would be adopted for the source. The source-selection

step is intended to add flexibility and discretion to the state planning process – ultimately, the state decides which sources to consider for reasonable progress.”

In the 2022 RH SIP, DEC chose not to perform a full four-factor analysis on the Healy Power Plant because the two coal-fired boilers already have SO<sub>2</sub> emissions controls. Additionally, EU 1 had already gone through a BART analysis during the first implementation period RH SIP that found additional SO<sub>2</sub> controls on the EU to be cost ineffective and, at the time of the 2022 RH SIP, it was possible that EU 1 would be retired in the future (which ended up not being the case as discussed above). In the case of EU 2, the coal-fired boiler has an emissions limit of 0.10 lb/MMBtu with a requirement to operate SDA on the EU. This emissions limit is half the emissions limit given in the 2019 Guidance Document’s example of a coal-fired boiler electrical generating unit that is equipped with flue gas desulfurization (which includes DSI and SDA) that meets a 0.2 lb/MMBtu emission rate. Although EU 1 had a less stringent emissions limit of 0.30 lb/MMBtu, the boiler was equipped with DSI using sodium bicarbonate, which the EPA Air Pollution Control Cost Manual estimates can achieve control efficiencies of 50 to 70%.<sup>6</sup> The emissions data reported via the NEI from the continuous emissions monitoring system for EU 1 over the previous three-year period for which data is available (2017-2019) showed an average SO<sub>2</sub> emissions rate of 0.26 lb/MMBtu.

In the 2022 RH SIP, DEC concluded that Unit 1 would be considered an effectively controlled source if an enforceable limit of 0.20 lb/MMBtu was selected. While lower emission limits may be achieved with DSI optimization, the selection of 0.20 lb/MMBtu represents significant emissions reductions that could be achieved cost-effectively in the relative near-term that would add greatly to the air quality of the region as well as further assist long term visibility impairment in the park, an issue that has not been shown to have any direct connection to emissions from Unit 1.

The 2010 Regional Haze BART determination<sup>7</sup> for Healy Power Plant’s EU 1 found that the incremental cost effectiveness for the addition of a spray dry absorber system was \$29,813 per ton of SO<sub>2</sub> removed and for a wet scrubber system was \$12,033 per ton of SO<sub>2</sub> removed. In line with the 2019 Guidance Document, DEC believed that there have been no significant cost reductions in the previous decade that would warrant re-evaluating the addition of these two types of controls for EU 1 as they would still be considered cost ineffective. However, the previous BART determination found that optimizing the already installed DSI system on EU 1 would cost \$4,218 per ton of SO<sub>2</sub> removed. It was possible that a re-evaluation of DSI optimization for EU 1 could result in a cost effectiveness finding by DEC. Therefore, in the 2022 RH SIP, DEC required that GVEA either retire EU 1 according to the CD (Option 1), complete a full four-factor analysis for DSI optimization and submit the final four factor analysis to DEC by July 1, 2023 (Option 2), or establish an enforceable emission limit for SO<sub>2</sub> of 0.20 lb/MMBtu by submitting an application for a permit amendment by January 1, 2024 (Option 3). This finding is summarized below in Table O.

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<sup>6</sup> EPA Air Pollution Control Cost Manual Section 5 SO<sub>2</sub> and Acid Gas Controls Chapter 1.2.1.3: <https://www.regulations.gov/document?D=EPA-HQ-OAR-2015-0341-0082>.

<sup>7</sup> See the Appendix III.K.6 Best Available Retrofit Technology (BART) Documentation PDF on DEC’s website: <https://dec.alaska.gov/air/anpms/regional-haze/sip/>.

**Table O - 2022 RH SIP Final Determination for GVEA – Healy Power Plant**

| <b>Pollutant</b>  | <b>Regional Haze Controls</b>   | <b>Regional Haze Determination</b>                        | <b>Effective Dates of Control/Limit</b>   |
|---|---|---|---|
| <b>EU 1 – Coal-Fired Boiler with DSI - 327 MMBtu/hr</b> |   |   |   |
| SO <sub>2</sub>   | Option 1 – Consent Decree   | Retire EU 1 by December 31, 2024                          | Decision by December 31, 2022<br><br>Retirement effective no later than December 31, 2024     |
|   | Option 2 – Four Factor Analysis   | Submit a four-factor analysis for DSI optimization to DEC | Submit Four-Factor Analysis by July 1, 2023   |
|   | Option 3 – Enforceable Limit  | Establish enforceable emission limit of 0.20 lb/MMBtu     | Submit permit application by January 1, 2024<br><br>Expect permit issuance by January 1, 2025 |
| <b>EU 2 – Coal-Fired Boiler with SDA - 658 MMBtu/hr</b> |   |   |   |
| SO <sub>2</sub>   | Already Effectively Controlled<br>(0.10 lb/MMBtu emission rate with Spray Dry Absorber) | No Additional Controls                                    | N/A   |

**2025 RH Updated Cost Analysis**

To fulfill its obligations outlined in the 2022 SIP, as discussed above, GVEA submitted a four-factor analysis for optimizing DSI on June 30, 2023, with the conclusion that their DSI system could not achieve an SO<sub>2</sub> emissions rate lower than EU 1’s current emissions limit of 0.30 lb/MMBtu through increased sorbent injection rates alone.

In this updated 2025 cost analysis, to calculate if DSI optimization could be considered cost effective, DEC chose to analyze recent BACT determinations made for SO<sub>2</sub> emissions controls from the 2024 Amendments to the FNSB NAA SIP, Appendix III.D.7.07.<sup>8</sup> In the BACT analyses for the FNSB NAA SIP, DSI was shown to be the most cost effective SO<sub>2</sub> emissions control technology available. Therefore, that is the only emissions control technology that was compared to Healy Power Plant’s EU 1. Table P below shows the Department’s 2024 DSI cost calculations for the coal-fired boilers located at Fort Wainwright, the Chena Power Plant, and the UAF Campus.

<sup>8</sup> The FNSB NAA SIP Appendix III.D.7.07 can be found at <https://dec.alaska.gov/air/anpms/sip/2024-fbks-pm2-5-serious-sip-amends/>.

**Table P - DEC Economic Analysis for Technically Feasible SO<sub>2</sub> Controls in the 2024 Amendments to the FNSB NAA SIP<sup>8</sup>**

| Source   | Total Rated Capacity (MMBtu/hr) | Uncontrolled PTE (tpy) | Emission Reduction (tpy) | Control Efficiency (%) | Total Capital Investment (\$) | Total Annual Costs (\$/year) | Cost Effectiveness (\$/ton) |
|--|---------------------------------|------------------------|--------------------------|------------------------|-------------------------------|------------------------------|-----------------------------|
| Fort Wainwright  | 1,380                           | 1,470.0                | 1369.0                   | 93                     | 28,424,000                    | 9,082,000                    | 6,636                       |
| UAF (Tri-Mer)  | 295.6                           | 129.5                  | 103.6                    | 80                     | 3,668,667                     | 4,223,707                    | 40,778                      |
| UAF (BACT, Inc.)   | 295.6                           | 129.5                  | 90.6                     | 70                     | 14,411,039                    | 3,203,706                    | 35,349                      |
| Chena Power Plant  | 497                             | 639.5                  | 607.6                    | 95                     | 43,809,891                    | 8,122,262                    | 13,368                      |
| Average  | 617                             | 592.1                  | 548.7                    | 92                     | 22,578,399                    | 6,157,919                    | 24,033                      |
| Capital Recovery Factor = 0.0931 (8.5% interest rate for a 30-year equipment life) |                                 |                        |                          |                        |                               |                              |                             |

In addition to the direct comparison shown in Table P above, DEC also used some of the costs and emissions reductions information from the FNSB NAA SIP and extrapolated the data for a comparison to Healy Power Plant's EU 1, as can be seen below in Table Q. Of the three sources with coal-fired boilers that were analyzed in the FNSB NAA SIP, only the UAF Campus's EU 113, rated at 295.6 MMBtu/hr, and the Chena Power Plant's EUs 4 through 7, rated at 485.1 MMBtu/hr (combined), were brought forward for comparison with Healy Power Plant's EU 1, which is rated at 327 MMBtu/hr. Fort Wainwright's EUs 1 through 6 have a combined rating of 1,380 MMBtu/hr, which is approximately four times the heat input of Healy Power Plant's EU 1.

For the analysis shown in Table Q below, DEC included the total capital investment and total cost data for DSI from the Chena Power Plant and UAF Campus from Table P above and included a row that averages the three. Additionally, DEC used the original control efficiencies from these source's economic analyses, which includes a higher emissions reduction percentage for both of UAF Campus's DSI analyses. DEC had lowered the baseline emissions rate in our BACT analysis for UAF Campus's EU 113 and therefore reduced the previous control efficiencies in order to keep the controlled emission factors the same as the vendor quotes provided to DEC. Additionally, DEC used the 245.4 tons of SO<sub>2</sub> emissions that GVEA reported for Healy Power Plant's EU 1 in the 2023 NEI for the analysis.

**Table Q - DEC Economic Analysis for Technically Feasible SO<sub>2</sub> Controls in the 2024 Amendments to the FNSB NAA SIP Compared to Healy Power Plant's EU 1<sup>8</sup>**

| Source            | 2023 Emissions (tpy) | Emission Reduction (tpy) | Control Efficiency (%) | Total Capital Investment (\$) | Total Annual Costs (\$/year) | Cost Effectiveness (\$/ton) |
|-------------------|----------------------|--------------------------|------------------------|-------------------------------|------------------------------|-----------------------------|
| UAF (Tri-Mer)     | 245.4                | 220.9                    | 90                     | 3,668,667                     | 4,223,707                    | 19,124                      |
| UAF (BACT, Inc.)  | 245.4                | 208.6                    | 85                     | 14,411,039                    | 3,203,706                    | 15,359                      |
| Chena Power Plant | 245.4                | 233.2                    | 95                     | 43,809,891                    | 8,122,262                    | 34,836                      |

| Source   | 2023 Emissions (tpy) | Emission Reduction (tpy) | Control Efficiency (%) | Total Capital Investment (\$) | Total Annual Costs (\$/year) | Cost Effectiveness (\$/ton) |
|--|----------------------|--------------------------|------------------------|-------------------------------|------------------------------|-----------------------------|
| Average  | 245.4                | 220.9                    | 90                     | 20,629,866                    | 5,183,225                    | 23,467                      |
| Capital Recovery Factor = 0.0931 (8.5% interest rate for a 30-year equipment life) |                      |                          |                        |                               |                              |                             |

As can be seen from Table Q above, the projected costs per ton of installing a new state-of-the-art DSI system capable of achieving 85 to 95% SO<sub>2</sub> emissions reductions on Healy Power Plant's EU 1 are in the range of 15 to 35 thousand dollars per ton of pollutant removed. It is possible that because Healy Power Plant's EU 1 already operates with an older DSI system, that the costs would not be as high as they likely already incur some of the same costs associated with this analysis. However, it is also possible that because Healy Power Plant's EU 1 already operates a DSI system, they would not be able to achieve SO<sub>2</sub> emissions reductions in the range of 85% to 95%. Therefore, in this updated 2025 cost analysis, DEC concludes that it would not be cost effective to optimize the DSI system on Healy's EU 1 to require a lower emissions rate.

#### **DEC's 2025 Regional Haze Findings for Healy Power Plant**

DEC finds that it is cost ineffective to upgrade the DSI control system on Healy Power Plant's coal-fired boiler EU 1 to lower the SO<sub>2</sub> emissions rate. Healy Power Plant's coal-fired boiler EU 2 is already considered "effectively controlled" under the 2019 Guidance Document with a requirement to operate EU 2 with flue gas desulfurization and a 0.1 lb/MMBtu SO<sub>2</sub> limit.<sup>9</sup> Therefore, no further emissions reductions or emissions controls are selected for the Healy Power Plant for the updated 2025 source review.

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<sup>9</sup> Condition 44 of Operating Permit AQ0173TVP03 limits EU 2 to an SO<sub>2</sub> emissions rate of not more than 0.10 lb/MMBtu.

### c. Aurora Energy, LLC: Chena Power Plant

#### Introduction and 2022 RH SIP Findings

The Chena Power Plant is an electric generating facility owned and operated by Aurora Energy, LLC (Aurora), and Aurora is the permittee for the stationary source's Title V Operating Permit AQ0315TVP04 Revision 1. The SIC code for this stationary source is 4911 - Electric Services. The Chena Power Plant is a co-generation power plant that is designed to supply the local power grid with up to 27.5 megawatts of electrical power and provide steam and hot water heat to commercial and residential customers in the city of Fairbanks. The power producing units consist of four coal-fired boilers. These EUs are listed below in Table R and Table S.

**Table R - Chena Power Plant Emission Unit Inventory**

| EU ID | Emissions Unit Name       | Emissions Unit Description     | Rating/Size             | Installation or Construction Date |
|-------|---------------------------|--------------------------------|-------------------------|-----------------------------------|
| 1     | Coal Preparation Plant    | Exhaust and Fugitive Emissions | 75 tons/hour            | 1950 <sup>1</sup>                 |
| 2     | Coal Stockpile            | Fugitive Emissions             | 0.59 acre               | 1950 <sup>2</sup>                 |
| 3     | Ash Vacuum Pump Exhaust   | Ash System Baghouse Exhaust    | 24,187 tons/yr (of ash) | 1997                              |
| 4     | Chena 1 Coal-Fired Boiler | Full Stream Baghouse Exhaust   | 76.8 MMBtu/hr           | 1952                              |
| 5     | Chena 2 Coal-Fired Boiler | Full Stream Baghouse Exhaust   | 76.8 MMBtu/hr           | 1952                              |
| 6     | Chena 3 Coal-Fired Boiler | Full Stream Baghouse Exhaust   | 76.8 MMBtu/hr           | 1954                              |
| 7     | Chena 5 Coal-Fired Boiler | Full Stream Baghouse Exhaust   | 254.7 MMBtu/hr          | 1970                              |

Table Notes: <sup>1</sup> EU ID 1 was modified in 1990.

<sup>2</sup> EU ID 2 was modified in 2013.

**Table S - Chena Power Plant Fugitive Emission Unit Inventory**

| EU ID | Emissions Unit Name   | Emissions Unit Description          | Rating/Size | Installation or Construction Date |
|-------|-----------------------|-------------------------------------|-------------|-----------------------------------|
| 8     | Truck Bay Ash Loadout | Bottom of silo – Fugitive Emissions | N/A         | 1952                              |
| 9     | Paved Roadways        | Fugitive Emissions                  | N/A         | 1950                              |

For the 2022 RH SIP analysis for the Chena Power Plant, DEC relied upon findings contained in the FNSB NAA SIP that resulted in the 2022 RH SIP determination summarized below in Table T. However, the SO<sub>2</sub> BACT requirements contained in the 2019/2020 FNSB NAA SIP were withdrawn by DEC on September 25, 2023. An updated BACT analysis was included with the

submittal of the 2024 FNSB SIP Amendment,<sup>10</sup> which contained a major source precursor demonstration for SO<sub>2</sub> emissions. Therefore, for the updated 2025 source review, DEC has relied upon additional BACT information for SO<sub>2</sub> emissions controls that was included as part of the 2024 FNSB SIP Amendment.<sup>10</sup>

**Table T - 2022 RH SIP Final Determination for Chena Power Plant**

| Pollutant   | Regional Haze Controls   | Regional Haze Determination | Effective Dates of Control/Limit |
|---|--|-----------------------------|----------------------------------|
| <i>EUs 4 through 7 - Coal-Fired Boilers - 497 MMBtu/hr (combined)</i> |  |                             |                                  |
| SO <sub>2</sub>   | Already Effectively Controlled (0.301 lb/MMBtu; 0.25% sulfur be weight in coal)* | No Additional Controls      | N/A                              |

### 2024 FNSB NAA SIP Amendment BACT Analysis

Section II.B.3.f. of the 2019 Guidance Document discusses selecting sources that have recently undergone emission control technology review. The 2019 Guidance Document states the following:

“New, reconstructed, or modified emission units that went through Best Available Control Technology (BACT) review under the Prevention of Significant Deterioration (PSD) program or Lowest Achievable Emission Rate (LAER) review under the nonattainment new source review program for major sources and received a construction permit on or after July 31, 2013, on a pollutant-specific basis. The statutory considerations for selection of BACT and LAER are also similar to, if not more stringent than, the four statutory factors for reasonable progress.”

The 2024 FNSB SIP Amendment<sup>11</sup> includes an SO<sub>2</sub> BACT analysis completed by DEC for Chena Power Plant’s coal-fired boilers under Part 2 of Appendix III.D.7.07. This analysis concluded that due to space constraints at the Chena Power Plant, it would not be technically feasible to install wet flue gas desulfurization (WFGD), circulating dry scrubbers (CDS), or spray dry absorbers (SDA) on coal-fired boilers. Therefore, dry sorbent injection (DSI) was advanced as the only possible control option for the coal-fired boilers. DEC’s economic analysis for DSI is shown below in Table U.

**Table U - DEC 2024 FNSB NAA SIP BACT Analysis for Chena Power Plant**

| Control Alternative   | Potential to Emit (tpy) | Emission Reduction (tpy) | Total Capital Investment (\$) | Total Annualized Costs (\$/year) | Cost Effectiveness (\$/ton) |
|---|-------------------------|--------------------------|-------------------------------|----------------------------------|-----------------------------|
| Dry Sorbent Injection   | 639.5                   | 607.6                    | 43,809,891                    | 8,122,262                        | 13,368                      |
| Capital Recovery Factor = 0.0931 of total capital investment ( $CRF = i(1+i)^n / ((1+i)^n - 1)$ [CCM Section 1, Chapter 2, page 22] with an interest rate of 8.5% for a 30-year life cycle) |                         |                          |                               |                                  |                             |

<sup>10</sup> DEC’s 2024 FNSB NAA SIP Amendment: <https://dec.alaska.gov/air/anpms/communities/fbks-pm2-5-2024-amendment-serious-sip/>.

<sup>11</sup> DEC’s 2024 FNSB NAA SIP Amendment: <https://dec.alaska.gov/air/anpms/communities/fbks-pm2-5-2024-amendment-serious-sip/>.



As can be seen in Table U above, DEC concluded that the average cost per ton of SO<sub>2</sub> removal would be \$13,368. Additionally, this BACT calculation for the FNSB NAA SIP was performed with the source's PTE used as the baseline emissions rate as opposed to actual emissions which are used for four-factor analyses in RH. If DEC updated this calculation with the 228.6 tons of actual SO<sub>2</sub> emissions emitted from the Chena Power Plant in 2023, this \$13,368 value would more than double. Therefore, DEC concludes that it would be too expensive to install DSI on the coal-fired boilers at the Chena Power Plant for the updated 2025 review.

#### **DEC 2025 Regional Haze Findings for Chena Power Plant**

DEC finds that it is technically infeasible to install WFGD, CDS, or SDA based on space constraints, and it is not cost effective to install DSI on the coal-fired boilers at the Chena Power Plant. Therefore, no further emissions reductions or emissions controls are selected for the Chena Power Plant in the updated 2025 source review.

**d. US Air Force: Eielson Air Force Base**

**Introduction and 2022 RH SIP Findings**

The Eielson Air Force Base (Eielson AFB) is owned and operated by the United States Air Force (USAF), and the USAF is the permittee for the stationary source's Title V Operating Permit AQ0264TVP02 Revision 5. The SIC code for this stationary source is 9711 – National Security. Eielson AFB consists of an operational airfield, residential housing, office buildings, gas stations, utilities, military police and fire departments, public schools, chapels, hospital facilities, retail stores, recreational facilities, and more. The stationary source's EUs are listed below in Table V.

**Table V - Eielson Air Force Base Emission Unit Inventory**

| <b>EU ID</b>                          | <b>Emission Unit Name</b>            | <b>Emission Unit Description</b> | <b>Rating/Size</b> | <b>Install Date</b> |
|---------------------------------------|--------------------------------------|----------------------------------|--------------------|---------------------|
| <b>Coal Fired Boilers<sup>1</sup></b> |                                      |                                  |                    |                     |
| 1                                     | CH&PP Main Boiler #1                 | Springfield Boiler               | 120,000 lb/hr      | 1952                |
| 2                                     | CH&PP Main Boiler #2                 | Springfield Boiler               | 120,000 lb/hr      | 1952                |
| 3                                     | CH&PP Main Boiler #3                 | Springfield Boiler               | 120,000 lb/hr      | 1952                |
| 4                                     | CH&PP Main Boiler #4                 | Springfield Boiler               | 120,000 lb/hr      | 1952                |
| 5A                                    | CH&PP Main Replacement Boiler #5     | Coal-Fired Boiler                | 120,000 lb/hr      | 2016                |
| 6A                                    | CH&PP Main Replacement Boiler #6     | Coal-Fired Boiler                | 120,000 lb/hr      | 2014                |
| <b>Liquid Fuel Fired Boilers</b>      |                                      |                                  |                    |                     |
| 7                                     | Auxiliary Heating Plant Boiler #1    | Cleaver Brooks Boiler            | 58.7 MMBtu/hr      | 2002                |
| 8                                     | Auxiliary Heating Plant Boiler #2    | Cleaver Brooks Boiler            | 58.7 MMBtu/hr      | 2002                |
| 9                                     | Missile Storage Boiler #1            | Cleaver Brooks Boiler            | 3.3 MMBtu/hr       | 1991                |
| 10                                    | Missile Storage Boiler #2            | Cleaver Brooks Boiler            | 2.9 MMBtu/hr       | 1993                |
| 11                                    | Alert Hangar Boiler #1               | Cleaver Brooks Boiler            | 6.0 MMBtu/hr       | 2008                |
| 12                                    | Alert Hangar Boiler #2               | Cleaver Brooks Boiler            | 6.0 MMBtu/hr       | 2008                |
| 13                                    | Waste Water Treatment Boiler #12     | Cleaver Brooks Boiler            | 6.7 MMBtu/hr       | 2012                |
| 14                                    | Waste Water Treatment Boiler #2      | Cleaver Brooks Boiler            | 6.7 MMBtu/hr       | 2012                |
| 15                                    | Auxiliary Heating Plant II Boiler #1 | --TBD; Not Installed--           | 98 MMBtu/hr        | TBD                 |
| 16                                    | Auxiliary Heating Plant II Boiler #2 | --TBD; Not Installed--           | 98 MMBtu/hr        | TBD                 |

| EU ID  | Emission Unit Name                    | Emission Unit Description  | Rating/Size   | Install Date |
|--|---------------------------------------|----------------------------|---------------|--------------|
| <b>Propane Fired Heaters</b>                                 |                                       |                            |               |              |
| 17   | Corrosion Control Heater #1           | Midco Burner               | 17.0 MMBtu/hr | 1987         |
| 18   | Corrosion Control Heater #2           | Midco Burner               | 17.0 MMBtu/hr | 1987         |
| <b>Diesel and Gasoline Fired Internal Combustion Engines</b> |                                       |                            |               |              |
| 19   | CH&PP Main Auxiliary Generator        | EMD Diesel Engine          | 2,500 kW      | 1987         |
| 20   | CH&PP Auxiliary Power Generator #1    | Onan Diesel Engine         | 1,125 kW      | 1998         |
| 21   | CH&PP Auxiliary Power Generator #2    | Onan Diesel Engine         | 1,125 kW      | 1998         |
| 22   | CH&PP Auxiliary Power Generator #3    | Onan Diesel Engine         | 1,125 kW      | 1998         |
| 23   | CH&PP Auxiliary Power Generator #4    | Onan Diesel Engine         | 1,125 kW      | 1998         |
| 24   | Waste Water Treatment Generator       | Caterpillar Diesel Engine  | 500 kW        | 1994         |
| 25   | Central Avenue (Clinic) Generator     | Cummins Diesel Engine      | 300 kW        | 2006         |
| 26   | Refueling Station Generator-Oscar Row | Onan Diesel Engine         | 750 kW        | 1994         |
| 27   | Engineer Hill Generator               | Onan Diesel Engine         | 150 kW        | 1987         |
| 28   | Alert Hangar Generator                | Komatsu Diesel Engine      | 100 kW        | 1985         |
| 29   | Power Plant Fire Pump                 | Caterpillar Diesel Engine  | 196 hp        | 1987         |
| 30   | Missile Maintenance Generator         | Onan-Cummins Diesel Engine | 125 kW        | 2011         |
| 31   | Control Tower Generator               | Onan Diesel Engine         | 125 kW        | 2005         |
| 32   | Telephone Exchange Generator          | Cummins Diesel Engine      | 125 kW        | 2003         |
| 33   | Command Post Generator                | Cummins Diesel Engine      | 80 kW         | 2009         |
| 34   | Airfield Lighting Generator           | Onan Diesel Engine         | 300 kW        | 2003         |
| 35   | Fire Pump P8 (Thunder Dome #1)        | Cummins Diesel Engine      | 340 hp        | 1989         |
| 36   | Fire Pump P9 (Thunder Dome #2)        | Cummins Diesel Engine      | 340 hp        | 1989         |
| 37   | Fire Pump P10 (Thunder Dome #3)       | Cummins Diesel Engine      | 340 hp        | 1989         |
| 38   | Fire Pump P11 (F-16 Hangar Pump #1)   | Cummins Diesel Engine      | 340 hp        | 1986         |
| 39   | Fire Pump P12 (F-16 Hangar Pump #2)   | Cummins Diesel Engine      | 340 hp        | 1986         |

|              |   |                                  |                    |                     |
|--------------|---|----------------------------------|--------------------|---------------------|
| 40           | Fire Pump P13 (F-16 Hangar Pump #3)                 | Cummins Diesel Engine            | 340 hp             | 1986                |
| 41           | Fire Pump P19 (Hog Pen A-10s)                       | Detroit Diesel Engine            | 235 hp             | 1994                |
| 42           | Fire Pump P20 (Hog Pen A-10s)                       | Detroit Diesel Engine            | 235 hp             | 1994                |
| 43           | Fire Pump P6 – Fire Support                         | Caterpillar Diesel Engine        | 121 hp             | 1989                |
| <b>EU ID</b> | <b>Emission Unit Name</b>                           | <b>Emission Unit Description</b> | <b>Rating/Size</b> | <b>Install Date</b> |
| 44           | Fire Pump P5 – Fire Support                         | Caterpillar Diesel Engine        | 121 hp             | 1990                |
| 45           | Fire Pump P1 – Fire Support                         | Caterpillar Diesel Engine        | 121 hp             | 1989                |
| 46           | Taxi Way #3 Fire Pump                               | Caterpillar Diesel Engine        | 121 hp             | 1989                |
| 47           | Pumphouse #3 Fire Pump                              | Caterpillar Diesel Engine        | 121 hp             | 1989                |
| 48           | Fire Pump P2  | Caterpillar Diesel Engine        | 120 hp             | 1989                |
| 49           | Communications Squadron Emergency Generator         | Onan Diesel Engine               | 100 kW             | 2003                |
| 50           | Water Treatment Plant Generator                     | Cummins Diesel Engine            | 300 kW             | 2012                |
| 51           | Utilidor (Auxiliary Heat Plant) Emergency Generator | Onan Diesel Engine               | 500 kW             | 2002                |
| 52           | E-2 Complex Fuel Tank Emergency Generator           | Kohler Power Diesel Engine       | 475 kW             | 2002                |
| 53           | Fuel Hydrant System Emergency Generator             | Caterpillar Diesel Engine        | 556 kW             | 2002                |
| 54           | Joint Mobility Complex (JMC) Emergency Generator    | Cummins Diesel Engine            | 800 kW             | 2002                |
| 55           | North ILS Generator                                 | Onan Diesel Engine               | 60 kW              | 1993                |
| 56           | DET 460 Generator                                   | Cummins Diesel Engine            | 60 kW              | 2010                |
| 57           | Conventional Munitions Fire Pump #1                 | Detroit Diesel Engine            | 120 hp             | 1999                |
| 58           | Conventional Munitions Fire Pump #2                 | Detroit Diesel Engine            | 120 hp             | 1999                |
| 59           | New Security Forces Facility Generator (CSC)        | Cummins Diesel Engine            | 350 kW             | 2005                |
| 60           | Fire Stationary No. 1 Generator                     | Cummins Diesel Engine            | 80 kW              | 2003                |
| 61           | Base Supply Fire Pump                               | Cummins Diesel Engine            | 208 hp             | 1993                |
| 62           | 354 Wing MOC Generator                              | Cummins Diesel Engine            | 100 kW             | 2004                |
| 63           | F-Well pump   | Cummins Diesel Engine            | 230 hp             | 2010                |
| 65           | Aircraft Arrestor Engine NW3                        | Waukesha Gas Engine              | 65 hp              | 1970                |
| 66           | Aircraft Arrestor Engine NE                         | Waukesha Gas Engine              | 65 hp              | 1970                |
| 67           | Aircraft Arrestor Engine ¾ W                        | Waukesha Gas Engine              | 65 hp              | 1970                |
| 68           | Aircraft Arrestor Engine ¾ E                        | Waukesha Gas Engine              | 65 hp              | 1970                |

|   |   |  |                    |                     |
|---|---|--|--------------------|---------------------|
| 69  | Aircraft Arrestor Engine SE                 | Waukesha Gas Engine  | 65 hp              | 1970                |
| 70  | Aircraft Arrestor Engine SW                 | Waukesha Gas Engine  | 65 hp              | 1970                |
| 71  | Loop Refueling (Type III Hydrant) Generator | Cummins Diesel Engine<br>Emergency Generator                               | 450 kW             | 2006                |
| 73  | 4 Bay Loop Hangar                           | Cummins Diesel Engine  | 100 kW             | 2010                |
| 74  | 8 Bay Loop Hangar                           | Cummins Diesel Engine  | 200 kW             | 2010                |
| <b>EU ID</b>  | <b>Emission Unit Name</b>                   | <b>Emission Unit Description</b>   | <b>Rating/Size</b> | <b>Install Date</b> |
| 75  | Missile Maintenance Well Pump Generator     | Cummins Diesel Engine  | 60 kW              | 2006                |
| 76  | E-2 Farm Fire Pump Emergency Generator      | Deere Diesel Engine  | 120 hp             | 2005                |
| 77  | Dining Facility Emergency Generator         | Cummins Diesel Engine  | 230 kW             | 2010                |
| 78  | Red Flag Emergency Generator                | Cummins Diesel Engine  | 50 kW              | 2009                |
| 80  | Cooling Pond Generator                      | Cummins Diesel Engine  | 350 kW             | 2010                |
| <b>Hush House (Jet Engine Test Facility)</b>                                  |   |  |                    |                     |
| 81  | Hush House                                  | N/A  | N/A                | 1989                |
| <b>Portable Asphalt/Rock Crusher Diesel Fired Internal Combustion Engines</b> |   |  |                    |                     |
| 82  | Recycle Plant Engine                        | John Deere Diesel Engine   | 450 hp             | 2007                |
| 83  | Jaw Crusher Engine                          | John Deere Diesel Engine   | 450 hp             | 2008                |
| 84  | Hydrascreen Engine                          | Deutz Diesel Engine  | 96 hp              | 2007                |
| <b>Fire Training</b>  |   |  |                    |                     |
| 85  | Fire Training                               | Fire Training Burn   | N/A                | N/A                 |
| <b>Portable Asphalt/Rock Crusher Fugitives</b>                                |   |  |                    |                     |
| 86  | Crusher #1                                  | Cobra 1000 Recycling Plant   | 150 TPH            | 2007                |
| 87  | Conveyor Transfer Point #1                  | Transfer Point (Recycling Plant to Superior Stackable Conveyor)            | 150 TPH            | 2007                |
| 88  | Conveyor Transfer Point #2                  | Transfer Point (Superior Stackable conveyor to 683 Hydrascreen)            | 150 TPH            | 2007                |
| 89  | Screening                                   | Findlay 683 Hydrascreen  | 150 TPH            | 2007                |
| 90  | Conveyor Transfer Point #3                  | Transfer Point (683 Hydrascreen to Oversize Return Conveyor Belt)          | 50 TPH             | 2007                |
| 91  | Conveyor Transfer Point #4                  | Transfer Point (Oversize Conveyor Belt Return to Cobra 1000 Recycle Plant) | 50 TPH             | 2007                |

|  |                                     |   |                    |                     |
|--|-------------------------------------|---|--------------------|---------------------|
| 92                                       | Conveyor Transfer Point #5          | Transfer Point (683 Hydrascreen to Second Deck Oversize Return Conveyor Belt) | 50 TPH             | 2007                |
| 93                                       | Fines Screening                     | 683 Hydrascreen Fines Screen  | 100 TPH            | 2007                |
| 94                                       | Conveyor Transfer Point #6          | Transfer Point (Fines Screen to Fines Belt)                                   | 100 TPH            | 2007                |
| 95                                       | Conveyor Transfer Point #7          | Transfer Point (Fines Belt to Superior Radial Stacking Conveyor)              | 100 TPH            | 2007                |
| 96                                       | Conveyor Transfer Point #8          | Transfer Point (Conveyor Discharge onto Asphalt Pile)                         | 100 TPH            | 2007                |
| <b>EU ID</b>                             | <b>Emission Unit Name</b>           | <b>Emission Unit Description</b>  | <b>Rating/Size</b> | <b>Install Date</b> |
| 97                                       | Jaw Crusher Feed                    | Jaw Crusher Dump Point  | 150 TPH            | 2008                |
| 98                                       | Conveyer Transfer Point #9          | Transfer Point (Jaw Crusher Screen to Superior Conveyer # 1)                  | 100 TPH            | 2008                |
| 99                                       | Conveyer Transfer Point #10         | Transfer Point (Superior Conveyer # 1 to Superior Conveyer # 2)               | 100 TPH            | 2008                |
| 100                                      | Conveyer Transfer Point #11         | Transfer Point (Superior Conveyer # 2 discharge on to Asphalt Stockpile)      | 100 TPH            | 2008                |
| 101                                      | Crusher #2                          | Jaw Crusher   | 150 TPH            | 2008                |
| 102                                      | Conveyer Transfer Point #12         | Transfer Point (Jaw Crusher Conveyer to Recycling Plant Feed Conveyer)        | 150 TPH            | 2008                |
| 103                                      | Conveyer Transfer Point #13         | Transfer Point (Jaw Crusher Conveyer to Cobra 1000 Recycling Plant)           | 150 TPH            | 2008                |
| <b>Jet Kerosene (JP-8) Storage Tanks</b> |                                     |   |                    |                     |
| 104                                      | South Ramp Loop Tank #6167          | AST – Internal Floating Roof Tank   | 420,000 gal        | 2006                |
| 105                                      | South Ramp Loop Tank #6268          | AST – Internal Floating Roof Tank   | 420,000 gal        | 2006                |
| 106                                      | Tanker Row Tank #3241-5             | AST – Internal Floating Roof Tank   | 420,000 gal        | 2000                |
| 107                                      | Tanker Row Tank #3244-6             | AST – Internal Floating Roof Tank   | 420,000 gal        | 2000                |
| <b>Other Regulated Sources</b>           |                                     |   |                    |                     |
| 109                                      | Aircraft Corrosion Control Facility | Regulated Surface Coating   | N/A                | 1987                |
| 110                                      | Sandwich Belt Conveyer              | Regulated Coal Processing System  | N/A                | 1994                |

|   |                                  |   |                    |                     |
|---|----------------------------------|---|--------------------|---------------------|
| 111   | Coal Tripper System              | Coal Tripper system with 6 identical 2,500 cfm Pulse Jet Collector Bin Vent Filters | 150 TPH            | 2010                |
| <b>Insignificant CI RICE Subject to NESHAP Subpart ZZZZ</b>                 |                                  |   |                    |                     |
| 64A   | A Water Well Pump Generator5     | Cummins Diesel Engine   | 60 kW              | 2012                |
| 64B   | B Water Well Pump Generator      | Cummins Diesel Engine   | 60 kW              | 2012                |
| 112   | North Glideslope Generator       | Cummins Diesel Engine   | 23 kW              | 2001                |
| 113   | ASOS/GPS Generator               | Onan Diesel Engine  | 30 kW              | 2005                |
| 114   | Base Radio MARS Generator        | Onan Diesel Engine  | 35 kW              | 2003                |
| 115   | TACAN South Glideslope Generator | Onan Diesel Engine  | 35 kW              | 2005                |
| 116   | Lift Station Generator           | Cummins Diesel Engine   | 30 kW              | 1991                |
| 117   | South ILS Generator              | Onan Diesel Engine  | 35 kW              | 2005                |
| <b>EU ID</b>  | <b>Emission Unit Name</b>        | <b>Emission Unit Description</b>  | <b>Rating/Size</b> | <b>Install Date</b> |
| 118   | Quarry Hill Generator            | Deere Diesel Engine   | 26 kW              | 2004                |
| 119   | POL Control Generator            | Kubota Diesel Engine  | 20 kW              | 2010                |
| 120   | Consolidated Munitions Generator | Onan Diesel Engine  | 16 kW              | 1999                |
| 121   | CE Control Generator             | Onan Diesel Engine  | 6 kW               | 1985                |
| 122   | Fire Station #2 Generator        | John Deere Diesel Engine  | 55 kW              | 1997                |
| 123   | Emergency Wastewater Pump Engine | John Deere 4039D Diesel Engine  | 60 kW              | 1991                |
| 124   | Emergency Wastewater Pump Engine | John Deere 4045D Diesel Engine  | 63 kW              | 2008                |
| 125   | Emergency Wastewater Pump Engine | John Deere 4045D Diesel Engine  | 63kW               | 2008                |
| 129   | North Slope Relay Generator      | Cummins Diesel Engine   | 60 kW              | 2011                |
| <b>Insignificant Gasoline Storage Tanks Subject to NESHAP Subpart CCCCC</b> |                                  |   |                    |                     |
| 126   | Horizontal Gasoline Fuel Tank    | N/A   | 25,948 gallons     | 1987                |
| 127   | Horizontal Gasoline Fuel Tank    | N/A   | 25,948 gallons     | 1987                |
| 128   | Horizontal Gasoline Fuel Tank    | N/A   | 25,948 gallons     | 1987                |

Table Note: Minor Permit AQ0264MSS05 was issued on August 9, 2010, and authorizes the stationary source to replace the existing coal-fired boilers EUs 1 through 6 with new coal-fired boilers EUs 1A, 2A, and 4A through 6A.

For the 2022 RH SIP, DEC looked back over the previous six-year period (2014-2019) for which data was available to determine Eielson AFB's SO<sub>2</sub> emissions. Table WX shows SO<sub>2</sub> emissions



reported to DEC in emission fee estimates from 2014 through 2019. Additionally, the SO<sub>2</sub> emissions reported in the NEI for 2014 and 2017 (the only year that NEI information was available for the source during this window) are contained in Table W as a footnote. As can be seen, Table W shows that the majority of SO<sub>2</sub> emissions emitted from Eielson AFB are from the coal-fired boilers and, consequently, those were the only EUs that were carried forward for analysis.

**Table W - Eielson Air Force Base SO<sub>2</sub> Emissions**

| <b>Calendar Year</b> | <b>Coal-Fired Boilers<br/>SO<sub>2</sub> Emitted<br/>(tons)</b> | <b>Other EUs<br/>SO<sub>2</sub> Emitted<br/>(tons)</b> | <b>Total SO<sub>2</sub> Emitted<br/>(tons)</b> |
|----------------------|---|--|--|
| 2019                 | 237.98  | 3.66   | 241.64   |
| 2018                 | 211.77  | 3.20   | 214.97   |
| 2017                 | 238.90  | 1.70   | 240.60 <sup>1</sup>                            |
| 2016                 | 261.18  | 1.54   | 262.72   |
| 2015                 | 263.10  | 2.30   | 265.40   |
| 2014                 | 267.3   | 1.70   | 269.00 <sup>1</sup>                            |

Table Notes:

<sup>1</sup> USAF reported 262.81 tons of SO<sub>2</sub> emissions in the 2017 NEI and 268.05 tons of SO<sub>2</sub> emissions in the 2014 NEI.

In the 2022 RH SIP, DEC previously made the finding that the newer coal-fired boilers, EUs 5a and 6a, are already considered “effectively controlled” for SO<sub>2</sub> emissions under the 2019 Guidance Document with dry sorbent injection (DSI) and an existing emissions limit of 0.2 lb/MMBtu, and the older, uncontrolled, coal-fired boilers EUs 1 through 4 would either need to be retired by December 31, 2024, or the USAF would need to submit a four-factor analysis for SO<sub>2</sub> controls by July 1, 2023. The USAF chose not to retire EUs 1 through 4 and instead submitted a four-factor analysis on June 29, 2023, that analyzed wet flue gas desulfurization (Wet FGD), spray dry absorber (SDA), and DSI. The USAF and DEC four-factor analyses for the coal-fired boilers EUs 1 through 4 are contained in the following sections.

### **SO<sub>2</sub> Four-Factor Analysis**

Section 169A(g)(1) of the CAA lists four factors that must be taken into consideration in determining reasonable progress and states are required to consider those four factors (i.e., cost of compliance, time necessary for compliance, energy and non-air environmental impacts, and remaining useful life of the source) in the control analysis step.

### **Cost of Compliance for the Coal-Fired Boilers (EUs 1 through 4)**

The cost of compliance estimates the values of capital costs, annual operating and maintenance costs, annualized costs, and cost per ton of emission reductions that have been prepared according to EPA’s Air Pollution Control Cost Manual. Costs are expressed in terms of cost effectiveness in the standardized unit of dollars per ton of actual SO<sub>2</sub> emissions reduced. DEC used information from the USAF four-factor analysis submitted on June 29, 2023 to complete the cost of compliance analysis. In addition, DEC used information included in previous BACT determinations found in the RACT, BACT, & LAER Clearinghouse (RBLC) database; internet research; and BACT analyses submitted to DEC for the FNSB NAA SIP.

The RBLC was searched for all determinations in the last 10 years under the process code 11.110 Coal Combustion in Industrial Size Boilers and Furnaces. The search results for the coal-fired boilers are summarized in Table X.

**Table X - RBLC Summary of SO<sub>2</sub> Controls for Industrial Coal-Fired Boilers**

| <b>Control Technology</b>                         | <b>Number of Determinations</b> | <b>Emission Limits (lb/MMBtu)</b> |
|---|---------------------------------|-----------------------------------|
| Flue Gas Desulfurization / Scrubber / Spray Dryer | 10                              | 0.06 – 0.12                       |
| Limestone Injection                               | 10                              | 0.055 – 0.114                     |
| Low Sulfur Coal                                   | 4                               | 0.06 – 1.2                        |

### **RBLC Review**

A review of similar units in the RBLC indicates flue gas desulfurization, limestone injection, and low sulfur coal are the principle SO<sub>2</sub> control technologies installed on industrial coal-fired boilers. The lowest SO<sub>2</sub> emission rate in the RBLC is 0.055 lb/MMBtu.

### **Identification of SO<sub>2</sub> Control Technology for Coal-Fired Boilers**

From research, DEC identified the following technologies as available for control of SO<sub>2</sub> emissions from coal-fired boilers:

#### **Wet Scrubbers/Wet Flue Gas Desulfurization (WFGD)**

Post combustion flue gas desulfurization techniques can remove SO<sub>2</sub> formed during combustion by using an alkaline reagent to absorb SO<sub>2</sub> in the flue gas. Flue gasses can be treated using wet, dry, or semi-dry desulfurization processes. In the wet scrubbing system, flue gas is contacted with a solution or slurry of alkaline material in a vessel providing a relatively long residence time. The SO<sub>2</sub> in the flue reacts with the alkali solution or slurry by adsorption and/or absorption mechanisms to form liquid-phase salts. These salts are dried to about one percent free moisture by the heat in the flue gas. These solids are entrained in the flue gas and carried from the dryer to a PM collection device, such as a baghouse.

Most WFGD systems use a limestone slurry sorbent which reacts with the SO<sub>2</sub> and falls to the bottom of the absorber tower where it is collected. Wet FGD systems generally have the highest control efficiencies. New wet FGD systems can achieve SO<sub>2</sub> removal of 99% and HCl removal of over 95%. Packed tower wet FGD systems may achieve efficiencies as high as 99.9% for some pollutant-solvent systems.<sup>12</sup> The Department considers flue gas desulfurization with a wet scrubber a technically feasible control technology for the industrial coal-fired boilers.

#### **Spray Dry Absorbers (SDA)**

Spray Dry Absorbers are gas absorbers in which a small amount of water is mixed with the sorbent. Lime (CaO) is usually the sorbent used in the spray drying process, but hydrated lime (Ca(OH)<sub>2</sub>) is also used and can provide greater SO<sub>2</sub> removal. Slurry consisting of lime and recycled solids is atomized/sprayed into the absorber. The SO<sub>2</sub> in the flue gas is absorbed into the slurry and reacts

<sup>12</sup> EPA Air Pollution Control Cost Manual: Section 5 – SO<sub>2</sub> and Acid Gas Controls, Chapter 1, Page 1-9: <https://www.epa.gov/economic-and-cost-analysis-air-pollution-regulations/cost-reports-and-guidance-air-pollution#cost%20manual>.

with the lime and fly ash alkali to form calcium salts. The scrubbed gas then passes through a particulate control downstream of the spray drier where additional reactions and SO<sub>2</sub> removal may occur, especially in the filter cake of a fabric filter (baghouse). Spray dryers can achieve SO<sub>2</sub> removal efficiencies up to 95%,<sup>13</sup> depending on the type of coal burned. The Department considers flue gas desulfurization with an SDA system a technically feasible control technology for the industrial coal-fired boilers.

### **Circulating Dry Scrubbers (CDS)**

Similar to other dry flue gas desulfurization systems, the CDS system is located after the air preheater, and byproducts from the system are collected in an integrated fabric filter. Unlike the SDA systems, a CDS system is considered a circulating fluidized bed of hydrated lime reagent to remove SO<sub>2</sub> rather than an atomized lime slurry; however, similar chemical reaction kinetics are used in the SO<sub>2</sub> removal process. In a CDS system, flue gas is treated in a type of Dry Lime FGD system in which the waste gas stream passes through an absorber vessel where the flue gas stream flows through a fluidized bed of hydrated lime and recycled byproduct. Water is injected into the absorber through a venturi located at the base of the absorber for temperature control. Flue gas velocity through the vessel is maintained to keep the fluidized bed of particles suspended in the absorber. Water sprayed into the absorber cools the flue gas from approximately 300° F at the inlet to the scrubber to approximately 160° F at the outlet of the fabric filter. The hydrated lime absorbs SO<sub>2</sub> from the gas and forms calcium sulfite and calcium sulfate solids. The desulfurized flue gas passing out of the absorber contains solid sorbent mixed with the particulate matter, including reaction products, unreacted hydrated lime, calcium carbonate, and fly ash. The solid sorbent and particulate matter are collected by the fabric filter. CDS can achieve over 98% reduction in SO<sub>2</sub> and other acid gases.<sup>14</sup> The Department considers CDS a technically feasible control technology for the industrial coal-fired boilers.

### **Dry Sorbent Injection (DSI)**

Unlike the three other FGD systems, dry sorbent injection (DSI) is not a stand-alone, add-on air pollution control system but a modification to the combustion unit or ductwork. DSI systems inject a powdered alkaline reagent directly into the flue gas duct ahead of the particle collection device. Where hydrated lime is used as the reagent, the addition of water may be necessary to complete the chemical reaction. These reagents react with the sulfur (and other acid gases) in-flight and on the surfaces of the particle collection device. The products of reaction, unreacted reagent, and fly ash are collected at the bottom of the particle collection device and disposed of through the plants fly ash collection system. Reagents typically utilized in DSI systems include hydrated lime, Trona, and sodium bicarbonate. According to the EPA CCM<sup>15</sup> DSI can achieve SO<sub>2</sub> control efficiencies ranging from 50 to 70% and has been used in power plants, biomass boilers, and industrial applications (e.g., metallurgical industries). However, USAF's four-factor analysis includes a 90% control efficiency for DSI, which is comparable to the removal efficiencies used in DEC's recent BACT analysis for the

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<sup>13</sup> EPA Air Pollution Control Cost Manual: Section 5 – SO<sub>2</sub> and Acid Gas Controls, Chapter 1, Table 1.3: <https://www.epa.gov/economic-and-cost-analysis-air-pollution-regulations/cost-reports-and-guidance-air-pollution#cost%20manual>.

<sup>14</sup> EPA Air Pollution Control Cost Manual: Section 5 – SO<sub>2</sub> and Acid Gas Controls, Chapter 1, Page 1-11: <https://www.epa.gov/economic-and-cost-analysis-air-pollution-regulations/cost-reports-and-guidance-air-pollution#cost%20manual>.

<sup>15</sup> EPA Air Pollution Control Cost Manual: Section 5 – SO<sub>2</sub> and Acid Gas Controls, Chapter 1, Page 1-11: <https://www.epa.gov/economic-and-cost-analysis-air-pollution-regulations/cost-reports-and-guidance-air-pollution#cost%20manual>.

FNSB NAA SIP. The Department considers DSI to be a technologically feasible control technology for the industrial coal-fired boilers.

### **Low Sulfur Coal**

The USAF purchases coal from the Usibelli Coal Mine located in Healy, Alaska. This coal mine is located 115 miles south of Fairbanks. The coal mined at Usibelli is sub-bituminous coal and has a relatively low sulfur content with guarantees of less than 0.4 percent by weight. Usibelli Coal Data Sheets indicate a range of 0.08 to 0.28 percent Gross as Received (GAR) percent Sulfur (%S). According to the U.S. Geological Survey, coal with less than one percent sulfur is classified as low sulfur coal. The Department considers the use of low sulfur coal a feasible control technology for the industrial coal-fired boilers. Because the Permittee already combusts low sulfur coal, this control option represents the baseline emissions rate, or a 0% emissions control.

### **Good Combustion Practices (GCPs)**

Good combustion practices for coal boilers include operator practices, maintenance knowledge, maintenance practices, adequate stoichiometric (fuel/air) ratio, combustion zone residence time, temperature, turbulence, fuel quality, combustion air distribution, fuel/waste dispersion. Proper management of the combustion process will result in a reduction of SO<sub>2</sub> emissions. The Department considers GCPs a technically feasible control option for the coal-fired boilers.

### **Eliminate Technically Infeasible SO<sub>2</sub> Technologies for the Coal-Fired Boilers**

None of the aforementioned control technologies were identified as being technically infeasible for the coal-fired boilers.

### **Rank the Remaining SO<sub>2</sub> Control Technologies for the Coal-Fired Boilers**

The following control technologies have been identified and ranked by efficiency for control of SO<sub>2</sub> emissions from the coal-fired boilers (Table Y):

**Table Y - Control Technologies**

| <b>Control Technology</b>        | <b>Control Level<sup>1,2</sup></b> |
|----------------------------------|------------------------------------|
| Wet Scrubbers (WFGD)             | 90% Control                        |
| Spray Dry Absorbers (SDA)        | 90% Control                        |
| Circulating Dry Scrubbers (CDS)  | 90% Control                        |
| Dry Sorbent Injection (DSI)      | 90% Control                        |
| Good Combustion Practices (GCPs) | Less than 40% Control              |
| Low Sulfur Coal                  | 0% Control (Baseline)              |

Table Notes:

<sup>1</sup>. The Department used the control efficiency provided in the USAF four-factor analysis for WFGD, SDA, and DSI.

<sup>2</sup>. Control technologies already required at the stationary source, including burning low sulfur coal or those included in the design of the EU are considered 0% control for the purposes of this four-factor analysis.

## Evaluate the Most Effective Controls

After identifying the control technologies and/or operating practices available for the coal-fired boilers, eliminating the technically infeasible control technologies and/or operating practices, and ranking the remaining control technologies and/or operating practices based on efficiency for control of SO<sub>2</sub> emissions, the next step is to perform a cost analysis for the remaining control technologies and/or operating practices. Below is the cost analysis provided by USAF, followed by DEC's own cost analysis.

### USAF Cost Analysis for SO<sub>2</sub> Emissions Controls from the Coal-Fired Boilers

The USAF provided an economic analysis for the use of WFGD, SDA, and DSI to control SO<sub>2</sub> emissions from the coal-fired boilers at Eielson AFB. The cost analysis used the EPA's cost control workbooks and associated guidance documents for SO<sub>2</sub> pollution control retrofits, April 2023 version.<sup>16</sup> For its analysis, the USAF used: an EU size of 16.7 MW as calculated by the monthly gross megawatt rating at full-load capacity, a usage rating of 50%, and a pre-control SO<sub>2</sub> E.F. of 0.20 lb/MMBtu which equated to uncontrolled SO<sub>2</sub> emissions of 69 to 72 tons per year; removal efficiencies of 90% for WFGD, SDA, and DSI; the default capital recovery factor (CRF) of 0.143 which equates to equipment life of 30 years and an interest rate of 14%, or an equipment life of 15 years and an interest rate of 11.5%; a waste disposal cost of \$50/ton; and an operating labor rate of \$63 per hour for DSI. Additionally, the USAF used a retrofit factor and location adjustment factor of 2.67 based on the latest Department of Defense Facilities Pricing Guide (Table 4-1 CONUS, of Unified Facilities Criteria 3-701-01, Change 2, dated 2 March 2023), which the USAF used "to better represent Eielson AFB's location, climate, on-site footprint limitations, and the capacity and condition of existing infrastructure and utilities available."

A summary of the USAF analysis for SO<sub>2</sub> controls for EUs 1 through 4 are shown below in Table Z. Note that the cost analysis is for each individual boiler in 2016 dollars.

**Table Z - USAF Economic Analysis for Technically Feasible SO<sub>2</sub> Controls for EUs 1 – 4**

| Control Alternative  | SO <sub>2</sub> Emissions (tons) | Emission Reduction (tpy) | Total Capital Investment (\$) | Total Annualized Costs (\$/year) | Cost Effectiveness (\$/ton) |
|--|----------------------------------|--------------------------|-------------------------------|----------------------------------|-----------------------------|
| WFGD   | 69                               | 63                       | 58,556,841                    | 10,217,000                       | 163,368                     |
| SDA  | 72                               | 65                       | 52,562,000                    | 8,825,000                        | 136,790                     |
| DSI  | 69                               | 62.5                     | 7,877,117                     | 1,779,000                        | 28,446                      |
| Capital Recovery Factor (CRF) = 0.143 of total capital investment ( $CRF = i(1+i)^n / ((1+i)^n - 1)$ )<br>CRF of 0.143 is equivalent to a 30-year equipment life (n) at 14% interest (i) |                                  |                          |                               |                                  |                             |

The USAF analysis also noted that the 2023 EPA retrofit spreadsheet uses 2016 dollars as the default value and so they included a correction to 2022 dollars and a plus or minus 30% cost estimate. These changes increased the cost effectiveness value for DSI, the most cost effective to \$32,446 per ton of SO<sub>2</sub> removed. The USAF concludes that the economic analysis indicates the level

<sup>16</sup> The April 2023 and April 2024 version of the EPA Retrofit Cost Tool can be found on EPA's website: <https://www.epa.gov/power-sector-modeling/retrofit-cost-analyzer>.

of SO<sub>2</sub> reduction does not justify the use of any SO<sub>2</sub> control for the coal-fired boilers based on the high implementation costs.

### DEC Cost Analysis for SO<sub>2</sub> Emissions Controls from the Coal-Fired Boilers

The Department revised the USAF economic analysis with EPA's April 2024 Retrofit Cost Tool spreadsheet<sup>16</sup> which uses 2024 dollars for WFGD and SDA and uses 2021 dollars for DSI. The Department performed two separate analyses to get a range of possible cost outcomes for the installation of SO<sub>2</sub> controls. For the high-cost estimate, the Department left the USAF inputs unchanged with the exception of increasing the usage capacity to 52% for WFGD and DSI to bring pre-control SO<sub>2</sub> emissions to 72 TPY, which matches the highest emissions from one of the coal-fired boilers in the 2023 NEI report. For the low-cost estimate, in addition to updating the April 2024 EPA Retrofit Tool and changing the usage factor, DEC also used the following default inputs to the EPA Retrofit Tool: a retrofit factor of 1.0; a control efficiency of 95% for WFGD and SDA, and 98% for DSI; a waste disposal cost of \$30 per ton; and an operating labor rate of \$60 per hour. In addition, in order to ensure a conservative low-cost estimate, DEC also changed the CRF to 0.0867, which represents the current bank prime interest rate of 7.75 percent<sup>17</sup> and a 30-year equipment life.

A summary of the DEC's analyses for SO<sub>2</sub> controls for EUs 1 through 4 are shown below in Table AA for the higher cost estimate and Table BB for the lower cost estimate. Note that both cost analyses are for each individual boiler.

**Table AA - DEC Economic Analysis for Technically Feasible SO<sub>2</sub> Controls for EUs 1 – 4**

| Control Alternative  | 2023 SO <sub>2</sub> Emissions (tons) | Emission Reduction (tpy) | Total Capital Investment (\$) | Total Annualized Costs (\$/year) | Cost Effectiveness (\$/ton) |
|--|---------------------------------------|--------------------------|-------------------------------|----------------------------------|-----------------------------|
| WFGD   | 72.3                                  | 65.0                     | 86,517,746                    | 14,324,000                       | 220,229                     |
| SDA  | 71.7                                  | 64.5                     | 77,640,000                    | 12,507,000                       | 193,863                     |
| DSI  | 72.3                                  | 65.0                     | 7,877,117                     | 1,794,000                        | 27,582                      |
| Capital Recovery Factor (CRF) = 0.143 of total capital investment ( $CRF = i(1+i)^n / ((1+i)^n - 1)$ )<br>CRF of 0.143 is equivalent to a 30-year equipment life (n) at 14% interest (i) |                                       |                          |                               |                                  |                             |

**Table BB - Department Economic Analysis for Technically Feasible SO<sub>2</sub> Controls for EUs 1 through 4**

| Control Alternative | 2023 SO <sub>2</sub> Emissions (tons) | Emission Reduction (tpy) | Total Capital Investment (\$) | Total Annualized Costs (\$/year) | Cost Effectiveness (\$/ton) |
|---------------------|---------------------------------------|--------------------------|-------------------------------|----------------------------------|-----------------------------|
| WFGD                | 72.3                                  | 68.7                     | 32,403,358                    | 4,760,000                        | 69,332                      |
| SDA                 | 71.7                                  | 68.1                     | 29,080,000                    | 3,923,000                        | 57,607                      |
| DSI                 | 72.3                                  | 70.8                     | 3,174,763                     | 861,000                          | 12,157                      |

<sup>17</sup> Bank prime interest rates from the Federal Reserve: <https://www.federalreserve.gov/releases/h15/>.

Capital Recovery Factor (CRF) =  $0.0632$  of total capital investment ( $CRF = i(1+i)^n / ((1+i)^n - 1)$ )  
 CRF of  $0.0867$  is equivalent to a 30-year equipment life ( $n$ ) at  $7.75\%$  interest ( $i$ )

DEC acknowledges that EPA's cost control workbooks published in April of 2023 and 2024, which were used for the analyses above, were designed for boilers that are larger than those found at Eielson AFB. Therefore, DEC also compared these costs to the SO<sub>2</sub> control costs recently published in the FNSB NAA SIP Appendix III.D.7.07<sup>18</sup> for Fort Wainwright. The coal-fired boilers at Fort Wainwright are similar sized units to those at Eielson AFB and both sets were installed in the 1950s. Table 5-3 from the 10.21.24 Fort Wainwright BACT Determination document is included below as Table CC.

**Table CC - Department Economic Analysis for Technically Feasible SO<sub>2</sub> Controls at Fort Wainwright**

| Control Alternative  | Potential to Emit (tpy) | Emission Reduction (tpy) | Total Capital Investment (\$) | Total Annual Costs (\$/year) | Cost Effectiveness (\$/ton) |
|--|-------------------------|--------------------------|-------------------------------|------------------------------|-----------------------------|
| WFGD - Caustic   | 101                     | 1369                     | 110,262,000                   | 18,832,000                   | 13,755                      |
| WFGD - limestone   | 101                     | 1369                     | 126,374,000                   | 19,474,000                   | 14,224                      |
| Spray-Dry Adsorption   | 176                     | 1293                     | 166,101,000                   | 22,812,000                   | 17,638                      |
| CDS  | 176                     | 1293                     | 196,447,000                   | 27,096,000                   | 20,950                      |
| Dry Sorbent Injection  | 101                     | 1369                     | 28,424,000                    | 9,082,000                    | 6,636                       |
| Capital Recovery Factor = 0.0931 (8.5% interest rate for a 30-year equipment life) |                         |                          |                               |                              |                             |

DEC notes that the BACT analysis for Fort Wainwright showed that the lowest cost per ton control was DSI with a 93% SO<sub>2</sub> removal rate, an SO<sub>2</sub> removal value of 1,369 tons per year, and with 1,470 tons of uncontrolled emissions (the sum of the Potential to Emit and the Emission Reduction columns). Meanwhile, the four-factor analysis for DSI at Eielson AFB was calculated with a conservative 98% SO<sub>2</sub> removal rate and 72.3 tons of uncontrolled emissions. DEC notes that EUs 1 through 4 at Eielson AFB had 212.3 tons of SO<sub>2</sub> emissions combined in 2023, which is approximately an order of magnitude less than the value used for the BACT analysis on the coal-boilers at Fort Wainwright that showed a cost per ton value of \$6,636. Therefore, DEC concludes that with such a substantial reduction in the numerator value of the cost per ton equation resulting from using actual emissions in the four-factor analysis vs potential emissions in the BACT analysis, the actual cost per ton for DSI at Eielson AFB is likely closer to the \$12,157 to \$27,582 value calculated in Table AA and Table BB, compared to the \$6,636 value in Table CC.

DEC's cost of compliance economic analysis indicates the level of SO<sub>2</sub> reduction does not justify the use of add on SO<sub>2</sub> controls for Eielson EUs 1 through 4 with an estimated cost of between \$12,157 to \$27,582 per ton of emission removed for DSI, the least expensive option. The Department notes that an economic analysis for CDS was not performed but recent cost analyses

<sup>18</sup> The FNSB NAA SIP Appendix III.D.7.07 can be found at <https://dec.alaska.gov/air/anpms/sip/2024-fbks-pm2-5-serious-sip-amends/>.

performed for coal-fired boilers in the FNSBNA SIP showed that CDS costs fall in between DSI and WFGD. Therefore, there is no emission limit or control selected for EUs 1 through 4 as a part of the updated 2025 source review.

#### **DEC 2025 Regional Haze Findings for Eielson Air Force Base**

DEC finds that it is cost ineffective to install any SO<sub>2</sub> controls on Eielson AFB's coal-fired boilers EUs 1 through 4. Eielson AFB's coal-fired boilers EUs 5A and 6A are already considered "effectively controlled" under the 2019 Guidance Document with flue gas desulfurization, plus 0.2 lb/MMBtu SO<sub>2</sub> limit.<sup>19</sup> Therefore, no further emissions reductions or emissions controls are selected for the Eielson Air Force Base for the updated 2025 source review.

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<sup>19</sup> 0.20 lb/MMBtu SO<sub>2</sub> limit is required under NSPS Subpart Db and is contained in Condition 54 of Operating Permit AQ0264TVP02 Rev. 4.



**e. U.S. Army, Doyon Utilities: Fort Wainwright**

**Introduction and 2022 RH SIP Findings**

Fort Wainwright is a military installation located within and adjacent to the city of Fairbanks, Alaska, in the Tanana River Valley. The EUs located within the military installation at Fort Wainwright are either owned and operated by a private utility company, Doyon Utilities, LLC. (DU) under Title V Operating Permit AQ1121TVP02 Revision 2, or by U.S. Army Garrison Fort Wainwright (Fort Wainwright or FWA) under Title V Operating Permit AQ0236TVP04. The two entities, DU and FWA, comprise a single stationary source operating under two permits. The stationary source includes coal-fired boilers for a combined heat and power plant, as well as emergency generator engines, fire pump engines, backup diesel fired boilers, and waste oil-fired boilers. These EUs are listed below in Table DD and Table EE.

**Table DD - DU Fort Wainwright Emission Unit Inventory**

| <b>EU ID1</b> | <b>Description of EU</b>                 | <b>Rating/Size</b> |          | <b>Location</b>                        |
|---------------|--|--------------------|----------|--|
| 1             | Coal-Fired Boiler 3                      | 230                | MMBtu/hr | Central Heating and Power Plant (CHPP) |
| 2             | Coal-Fired Boiler 4                      | 230                | MMBtu/hr | CHPP                                   |
| 3             | Coal-Fired Boiler 5                      | 230                | MMBtu/hr | CHPP                                   |
| 4             | Coal-Fired Boiler 6                      | 230                | MMBtu/hr | CHPP                                   |
| 5             | Coal-Fired Boiler 7                      | 230                | MMBtu/hr | CHPP                                   |
| 6             | Coal-Fired Boiler 8                      | 230                | MMBtu/hr | CHPP                                   |
| 7a            | South Coal Handling Dust Collector DC-01 | 13,150             | acfm     | CHPP                                   |
| 7b            | South Underbunker Dust Collector DC-02   | 884                | acfm     | CHPP                                   |
| 7c            | North Coal Handling Dust Collector NDC-1 | 9,250              | acfm     | CHPP                                   |
| 8             | Backup Generator Engine                  | 2,937              | hp       | CHPP                                   |
| 9             | Emergency Generator Engine               | 353                | hp       | Building 1032                          |
| 14            | Emergency Generator Engine               | 320                | hp       | Building 1563                          |
| 22            | Emergency Generator Engine               | 35                 | hp       | Building 3565                          |
| 23            | Emergency Generator Engine               | 155                | hp       | Building 3587                          |
| 29            | Emergency Pump Engine                    | 75                 | hp       | Building 1056                          |
| 30            | Emergency Pump Engine                    | 75                 | hp       | Building 3403                          |
| 31            | Emergency Pump Engine                    | 75                 | hp       | Building 3724                          |
| 32            | Emergency Pump Engine                    | 75                 | hp       | Building 4162                          |
| 33            | Emergency Pump Engine                    | 75                 | hp       | Building 1002                          |
| 34            | Emergency Pump Engine                    | 220                | hp       | Building 3405                          |

| EU ID1 | Description of EU              | Rating/Size |      | Location      |
|--------|--------------------------------|-------------|------|---------------|
| 35     | Emergency Pump Engine          | 55          | hp   | Building 4023 |
| 36     | Emergency Pump Engine          | 220         | hp   | Building 3563 |
| 51a    | DC-1 Fly Ash Dust Collector    | 3,620       | acfm | CHPP          |
| 51b    | DC-2 Bottom Ash Dust Collector | 3,620       | acfm | CHPP          |
| 52     | Coal Storage Pile              | N/A         |      | CHPP          |

**Table EE - U.S. Army Garrison Fort Wainwright Emission Unit Inventory**

| EU ID | Description of EU                  | Rating/Size |                      | Location        |
|-------|------------------------------------|-------------|----------------------|-----------------|
| 8     | Backup Diesel-Fired Boiler 1       | 19          | MMBtu/hr             | Basset Hospital |
| 9     | Backup Diesel-Fired Boiler 2       | 19          | MMBtu/hr             | Basset Hospital |
| 10    | Backup Diesel-Fired Boiler 3       | 19          | MMBtu/hr             | Basset Hospital |
| 11    | Backup Diesel-Electric Generator 1 | 900         | kW                   | Basset Hospital |
| 12    | Backup Diesel-Electric Generator 2 | 900         | kW                   | Basset Hospital |
| 13    | Backup Diesel-Electric Generator 3 | 900         | kW                   | Basset Hospital |
| 22    | VOC Extraction and Combustion      | N/A         |                      |                 |
| 23    | Fort Wainwright Landfill           | 1.97        | million cubic meters |                 |
| 24    | Aerospace Activities               | N/A         |                      |                 |
| 26    | Emergency Generator                | 324         | hp                   | Building 2132   |
| 27    | Emergency Generator                | 67          | hp                   | Building 1580   |
| 28    | Emergency Generator                | 398         | hp                   | Building 3406   |
| 29    | Emergency Generator                | 47          | hp                   | Building 3567   |
| 30    | Fire Pump                          | 275         | hp                   | Building 2089   |
| 31    | Fire Pump #1                       | 235         | hp                   | Building 1572   |
| 32    | Fire Pump #2                       | 235         | hp                   | Building 1572   |
| 33    | Fire Pump #3                       | 235         | hp                   | Building 1572   |
| 34    | Fire Pump #4                       | 235         | hp                   | Building 1572   |
| 35    | Fire Pump #1                       | 240         | hp                   | Building 2080   |
| 36    | Fire Pump #2                       | 240         | hp                   | Building 2080   |
| 37    | Fire Pump                          | 105         | kW                   | Building 3498   |
| 38    | Fire Pump #1                       | 120         | hp                   | Building 5009   |
| 39    | Fire Pump #2                       | 120         | hp                   | Building 5009   |
| 40    | Waste Oil-Fired Boiler             | 2.6         | MMBtu/hr             | Building 5007   |

| EU ID | Description of EU             | Rating/Size |        | Location      |
|-------|-------------------------------|-------------|--------|---------------|
| 50    | Emergency Generator Engine    | 762         | hp     | Building 1060 |
| 51    | Emergency Generator Engine    | 762         | hp     | Building 1060 |
| 52    | Emergency Generator Engine    | 82          | hp     | Building 1193 |
| 53    | Emergency Generator Engine    | 587         | hp     | Building 1555 |
| 54    | Emergency Generator Engine    | 1,059       | hp     | Building 2117 |
| 55    | Emergency Generator Engine    | 212         | hp     | Building 2117 |
| 56    | Emergency Generator Engine    | 176         | hp     | Building 2088 |
| 57    | Emergency Generator Engine    | 212         | hp     | Building 2296 |
| 58    | Emergency Generator Engine    | 71          | hp     | Building 3004 |
| 59    | Emergency Generator Engine    | 35          | hp     | Building 3028 |
| 60    | Emergency Generator Engine    | 95          | hp     | Building 3407 |
| 61    | Emergency Generator Engine    | 50          | hp     | Building 3703 |
| 62    | Emergency Generator Engine    | 18          | hp     | Building 5108 |
| 63    | Emergency Generator           | 68          | hp     | Building 1620 |
| 64    | Emergency Generator           | 274         | hp     | Building 1054 |
| 65    | Emergency Generator           | 274         | hp     | Building 4390 |
| ???   | Distillate Fired Boilers (23) | Varies      |        | Varies        |
| ???   | Waste Oil-Fired Boiler        | 2.5         | gal/hr | Building 3476 |
| ???   | Waste Oil-Fired Boiler        | 2.5         | gal/hr | Building 3476 |

For the 2022 RH SIP analysis for Fort Wainwright, DEC relied upon findings contained in the FNSB NAA SIP that resulted in the 2022 RH SIP determination summarized below in Table FF. However, the SO<sub>2</sub> BACT requirements contained in the 2019/2020 FNSB NAA SIP were withdrawn by DEC on September 25, 2023. An updated BACT analysis was included with the submittal of the 2024 FNSB SIP Amendment,<sup>20</sup> which contained a major source precursor demonstration for SO<sub>2</sub> emissions. Therefore, DEC has relied upon additional BACT information for SO<sub>2</sub> emissions controls that was included as part of the FNSB SIP Amendment.<sup>20</sup>

**Table FF - Final Determination for Fort Wainwright CHPP**

| Pollutant   | Regional Haze Controls   | Regional Haze Determination | Effective Dates of Control/Limit |
|---|--|-----------------------------|----------------------------------|
| <b>EUs 1 through 6 - Coal-Fired Boilers - 230 MMBtu/hr (each)</b> |  |                             |                                  |
| SO <sub>2</sub>   | Already Effectively Controlled (0.12 lb/MMBtu with DSI; 0.25% sulfur by weight in coal)* | No Additional Controls      | N/A                              |

<sup>20</sup> DEC's 2024 FNSB NAA SIP Amendment: <https://dec.alaska.gov/air/anpms/communities/fbks-pm2-5-2024-amendment-serious-sip/>.

\* Background and detailed information regarding Fairbanks PM<sub>2.5</sub> State Implementation Plan (SIP) can be found at <http://dec.alaska.gov/air/anpms/communities/fbks-pm2-5-serious-sip/>.

## 2024 FNSB NAA SIP Amendment BACT Analysis

Section II.B.3.f. of the 2019 Guidance Document discusses selecting sources that have recently undergone emission control technology review. The 2019 Guidance Document states the following:

“New, reconstructed, or modified emission units that went through Best Available Control Technology (BACT) review under the Prevention of Significant Deterioration (PSD) program or Lowest Achievable Emission Rate (LAER) review under the nonattainment new source review program for major sources and received a construction permit on or after July 31, 2013,<sup>46</sup> on a pollutant-specific basis. The statutory considerations for selection of BACT and LAER are also similar to, if not more stringent than, the four statutory factors for reasonable progress.”

The 2024 FNSB SIP Amendment<sup>21</sup> includes an SO<sub>2</sub> BACT analysis completed by DEC for Fort Wainwright’s coal-fired boilers under Part 3 of Appendix III.D.7.07. DEC’s SO<sub>2</sub> BACT analysis for Fort Wainwright covered the following control technologies: WFGD (caustic and limestone), SDA, CDS, and DSI. This SO<sub>2</sub> BACT analysis concluded that DSI was the only cost-effective control technology and, therefore, the Department at the time advanced DSI as the only possible cost-effective control option for Fort Wainwright’s six coal-fired boilers. DEC’s economic analysis for DSI is shown below in Table GG.

**Table GG - DEC 2024 FNSB NAA SIP BACT Analysis for Fort Wainwright**

| Control Alternative   | Potential to Emit (tpy) | Emission Reduction (tpy) | Total Capital Investment (\$) | Total Annual Costs (\$/year) | Cost Effectiveness (\$/ton) |
|---|-------------------------|--------------------------|-------------------------------|------------------------------|-----------------------------|
| WFGD - Caustic  | 101                     | 1369                     | 110,262,000                   | 18,832,000                   | 13,755                      |
| WFGD - limestone  | 101                     | 1369                     | 126,374,000                   | 19,474,000                   | 14,224                      |
| Spray-Dry Adsorption  | 176                     | 1293                     | 166,101,000                   | 22,812,000                   | 17,638                      |
| CDS   | 176                     | 1293                     | 196,447,000                   | 27,096,000                   | 20,950                      |
| Dry Sorbent Injection   | 101                     | 1369                     | 28,424,000                    | 9,082,000                    | 6,636                       |
| Capital Recovery Factor = 0.0931 of total capital investment ( $CRF = i(1+i)^n / ((1+i)^n - 1)$ [CCM Section 1, Chapter 2, page 22] with an interest rate of 8.5% for a 30-year life cycle) |                         |                          |                               |                              |                             |

As can be seen in Table GG above, DEC concluded that the average cost per ton of SO<sub>2</sub> removal would be \$6,636. However, this BACT analysis was performed with the source’s PTE used as the baseline emissions rate as opposed to the source’s actual emissions which are used for four-factor analyses in RH. If DEC updated this calculation to use the source’s actual emissions, 397.9 tons of actual SO<sub>2</sub> emissions emitted from the Chena Power Plant in 2023, instead of the 1,470 tons per

<sup>21</sup> DEC’s 2024 FNSB NAA SIP Amendment: <https://dec.alaska.gov/air/anpms/communities/fbks-pm2-5-2024-amendment-serious-sip/>.

year originally used for this analysis, the \$6,636 cost effectiveness value shown above in Table GG would more than triple. Therefore, DEC concludes that it would be too expensive to install DSI on the coal-fired boilers at the Fort Wainwright Power Plant for the updated 2025 source review.

#### **DEC Regional Haze Findings for Fort Wainwright CHPP**

DEC finds that it is economically infeasible to install WFGD, CDS, SDA, or DSI on the coal-fired boilers at the Fort Wainwright Power Plant. As the analysis shows, for the purpose of the updated 2025 source review, these SO<sub>2</sub> emissions controls are not cost-effective. Therefore, no further emissions reductions or emissions controls are selected for the Fort Wainwright Power Plant for the updated 2025 source review.

**Enclosure 2: Alaska's Class I Areas Visibility**

## **Enclosure 2: Alaska Class I Areas Visibility**

Many of the most significant impacts on Alaska's visibility are uncontrollable sources unique to the state. Visibility degradation contributors such as Alaska-specific vegetation fueling wildfires, episodic volcanic events, oceanic dimethyl sulfide, and international pollution including natural occurrences and emissions from passing international marine vessels are all factors that do not typically affect other Class I areas. Despite these additional impairments, Alaska's Class I areas have some of the greatest visibility and require the least improvement to achieve their 2064 Endpoint Goals under the Regional Haze Rule.

The report titled "2064 Endpoint Updated October 2023"<sup>1</sup> lists the Baselines and the 2064 Endpoint Goals for 113 IMPROVE monitoring stations across the United States. Of the reported stations, the baselines for Alaska's stations located in Denali National Park (DENA1 and TRCR1) and Tuxedni National Wildlife Refuge (KPBO1) are the closest to their respective 2064 Endpoint Goals. Less than three deciviews separate the two points at each station. Note an official baseline for KPBO1 has not yet been provided by EPA and only the 2064 Endpoint Goal is included in the report. However, DEC estimated KPBO1's baseline by averaging the first three years of average annual MID results, the same methodology used to calculate TRCR1 and SIME1's Baselines. The assumed KPBO1 Baseline was used to compare to the other station's data.

**Table 1. Baseline and Endpoint Visibility in Deciviews**

| <b>Class I Area</b>                      | <b>Denali National Park</b> | <b>Denali National Park</b> | <b>Tuxedni National Wildlife Refuge<sup>1</sup></b> | <b>Tuxedni National Wildlife Refuge<sup>2</sup></b> | <b>Simeonof National Wildlife Refuge</b> |
|--|-----------------------------|-----------------------------|---|---|--|
| <b>IMPROVE Station</b>                   | <b>DENA1</b>                | <b>TRCR1</b>                | <b>TUXE1</b>  | <b>KPBO1</b>  | <b>SIME1</b>                             |
| Baseline                                 | 7.08475                     | 9.11354                     | 10.46850  | 11.46634  | 13.66870                                 |
| 2064 Endpoint - Unadjusted <sup>3</sup>  | 4.72274                     | 6.35727                     | 6.96201   | 8.76500   | 8.50625                                  |
| Difference between Baseline and Endpoint | 2.36201                     | 2.75627                     | 3.50649   | 2.70134   | 5.16246                                  |

Table Notes:

<sup>1</sup>. TUXE1 stopped collecting data in December 2014 and was replaced by KPBO1.

<sup>2</sup>. KPBO1 replaced TUXE1 with the first full year of data collected being 2016. A baseline for the station has not been officially determined by EPA. Instead, DEC estimated the baseline by averaging the first three years of annual averages, the same technique used to determine the Baseline for TUXE1, TRCR1, and SIME1.

<sup>3</sup>. The 2064 End Point Goal or the natural visibility conditions is reported in the IMPROVE data reports called "URP Glidepath – M.I.D" report or the reported in the spreadsheet entitled 2064 Endpoint Updated October.

<https://views.cira.colostate.edu/fed/Express/AqrvTools.aspx#Visibility>

<http://vista.cira.colostate.edu/Improve/rhr-summary-data/>

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<sup>1</sup> Federal Land Manager Environmental Database-Interagency Monitoring of Protected Visual Environments. (October 2023). *2064 Endpoint Updated October 2023*. <http://vista.cira.colostate.edu/Improve/rhr-summary-data/>. (Accessed 9/11/2025)

The visibility in Alaska's Class I areas is even closer to the 2064 Endpoint Goals than Table 1 above reflects. The methodology and calculations used to designate emissions as either natural or anthropogenic do not have a mechanism to account for Alaska's unique uncontrollable emission sources impacting visibility. These emissions are mischaracterized as controllable anthropogenic and inflate the annual average visibility degradation values, making it impossible for Alaska to achieve the 2064 Endpoint Goals. This error is best illustrated with the data collected by the IMPROVE station representing Simeonof National Wildlife Refuge (Simeonof) designated as SIME1. The SIME1 station is located 60 miles northwest of Simeonof in Sand Point, a community of approximately 600 people on Popof Island in the Aleutian Chain. Simeonof is the farthest Class I area from Alaska's largest emission sources, the site is over 400 miles from the oil and gas operations in Cook Inlet and over 700 miles from the coal-fired power plants operating in the Fairbanks North Star Borough. The only industrial sources close to the station are a small, seasonally operated fish processing plant, and a small diesel generating facility. Yet, as shown in the table above, the station's Baseline and 2064 Endpoint Goal are almost double that of DENA1, the station closest to all the state's biggest coal-fired boilers.

Alaska is heavily impacted by both natural and anthropogenic emissions generated in the Russian Far East and Siberia, East Asia, Canada, and Europe. Emissions from passing international marine vessels impact Simeonof more than any of the other Class I areas. A gap in coverage leaves Simeonof outside of the North American Emission Control Area (ECA) established by the International Maritime Organization as part of the MARPOL convention. The ECA implemented a sulfur standard in 2015 limiting fuel oil burned in marine vessels to a maximum sulfur concentration of 0.5% in designated areas, a significant reduction from the previous limit of 3.5%. However, although the treaty limiting sulfur concentration for the North America ECA protects the shoreline for the rest of the United States, coverage extends to only a small portion of Alaska's coastline including the Inside Passage and the Gulf of Alaska. The Aleutian Islands, Western Alaska, and Northern Alaska are not included and many international vessels operating in these areas continue to burn heavy fuel oil high in sulfur.

Due to limited resources, Alaska is unable to conduct studies to quantify impacts from international emissions to properly categorize them as uncontrollable. Instead, to support Alaska, Hawaii, Puerto Rico, and the Virgin Islands in developing their Second RH Implementation Plan, EPA conducted hemispheric CMAQ modeling to estimate sulfate contributions from international anthropogenic emissions and commercial marine vessels. Based on the results, the report proposed an adjusted 2064 Endpoint and glidepath at each of the Class I areas by adding an estimate of the visibility impact from international anthropogenic sources to natural visibility conditions. The modeling and methodologies used by EPA to calculate the adjusted Endpoints are described in more detail in the report entitled, "Technical Support Document for EPA's Updated 2028 Regional Haze Modeling for Hawaii, Virgin Islands, and Alaska".

Table 2 provides the Baseline for each of Alaska's IMPROVE stations and provides both the Unadjusted and Adjusted 2064 End Points based on the modeling results. By adding the uncontrollable international sulfate emissions into the End Points, a more accurate comparison of the annual average visibility to the glidepath is possible. As shown, the differences between each station's Baseline and End Point decrease significantly to around 1.5 deciviews at DENA1, TRCR1, and KPBO1 and to less than one deciview at SIME1.



**Table 2. Baseline and Adjusted Endpoint Visibility in Deciviews**

| <b>Class I Area</b>                                 | <b>Denali National Park</b> | <b>Denali National Park</b> | <b>Tuxedni National Wildlife Refuge<sup>1</sup></b> | <b>Tuxedni National Wildlife Refuge<sup>2</sup></b> | <b>Simeonof National Wildlife Refuge</b> |
|---|-----------------------------|-----------------------------|---|---|--|
| <b>IMPROVE Station</b>                              | <b>DENA1</b>                | <b>TRCR1</b>                | <b>TUXE1</b>  | <b>KPBO1</b>  | <b>SIME1</b>                             |
| Baseline  | 7.08475                     | 9.11354                     | 10.46850  | 11.46634  | 13.66870                                 |
| 2064 Endpoint - Unadjusted <sup>3</sup>             | 4.72274                     | 6.35727                     | 6.96201   | 8.76500   | 8.50625                                  |
| 2064 Endpoint - Adjusted <sup>4</sup>               | 5.60                        | 7.55                        | 9.92  | 9.92  | 12.86                                    |
| Difference between Baseline and Endpoint - Adjusted | 1.48475                     | 1.56354                     | 0.54850   | 1.54634   | 0.80870                                  |

Table Notes:

- <sup>1.</sup> TUXE1 stopped collecting data in December 2014 and was replaced by KPBO1.
- <sup>2.</sup> KPBO1 replaced TUXE1 with the first full year of data collected being 2016. A baseline for the station has not been officially determined by EPA. Instead, DEC estimated the baseline by averaging the first three years of annual averages, the same technique used to determine the Baseline for TUXE1, TRCR1, and SIME1.
- <sup>3.</sup> The 2064 End Point Goal or the natural visibility conditions is reported in the IMPROVE data reports called “URP Glidepath – M.I.D” report or the reported in the spreadsheet entitled 2064 Endpoint Updated October.  
<https://views.cira.colostate.edu/fed/Express/AqrvTools.aspx#Visibility>  
<http://vista.cira.colostate.edu/Improve/rhr-summary-data/>
- <sup>4.</sup> Adjusted 2064 Endpoint values provided in Table 3-3 of the report entitled, “Technical Support Document for EPA’s Updated 2028 Regional Haze Modeling for Hawaii, Virgin Islands, and Alaska”. Both TUXE1 and KPOB1 stations were given the same adjusted Endpoint. However, DEC contends that due to the significant change in geographical location and emission source exposure, KPBO1 should be treated as a new site and the data set stand alone.

EPA’s modeling efforts also included a zero-out of U.S. anthropogenic emissions for a 2028 visibility projection at each Class I area. The zero-out U.S. anthropogenic emission simulations exclude any anthropogenic emission sources located in the U.S. or territories to provide visibility conditions caused by international anthropogenic emissions and natural sources that are beyond the control of states preparing the RH SIP. This included Class 1 and 2 commercial marine vessels but not Class 3 vessels. CMAQ model setup and all other inputs (i.e., meteorological fields, initial concentrations, and boundary concentrations) are unchanged from the 2016 base year simulation.

Figure 1 below displays the original glidepath as a blue line for each Class I area in Alaska and the adjusted glidepath as a yellow line. The unadjusted projected 2028 MID value is depicted with a solid black circle while the U.S. zero out 2028 forecast is depicted as a solid green circle. As depicted in the figures, modeling indicates that even after excluding all anthropogenic emissions, visibility at Alaska’s Class I areas remains above the glidepath at all four IMPROVE stations. In fact, the difference

between the 2028 unadjusted forecast and the 2028 zero-out MID is negligible and even undiscernible at Simeonof.

**Figure 1. Visibility Glidepaths and 2028 Forecasts in Deciviews at Each Alaska IMPROVE Station**

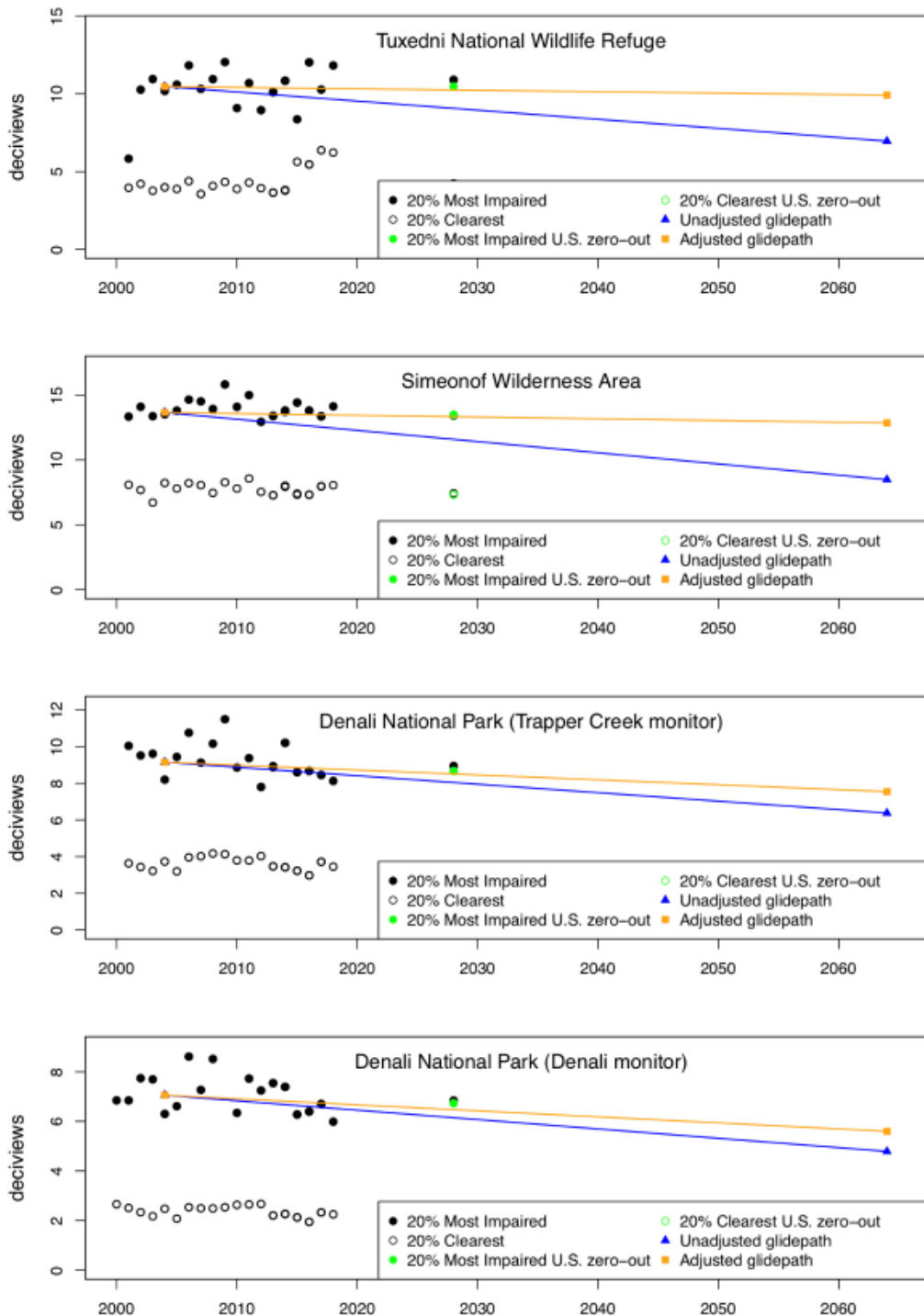


Figure Source: Technical Support Document for EPA's Updated 2028 Regional Haze Modeling for Hawaii, Virgin Islands, and Alaska, Figure 3.9-2. August 2021.

The results of EPA's modeling effort demonstrate that Alaska's Class I areas are already achieving natural visibility conditions. It also confirms that the methodology used to identify uncontrollable and natural sources of visibility impairment is insufficient to properly categorize sources unique to Alaska.

Even after accounting for the international anthropogenic emissions in the 2064 Endpoint and removing all U.S. anthropogenic sources to estimate the 2028 MID point, visibility forecasts remain above the glidepath at all four stations. The difference between Baseline and the 2064 Endpoint Goals can therefore be attributed to natural sources of impairment like Alaska-specific vegetation fueling wildfires, episodic volcanic events, and oceanic dimethyl sulfide.

The study further indicates that imposing additional emission restrictions on industrial sources such as the coal-fired boilers at the Golden Valley Electric Association Healy Power Plant or Eielson Air Force Base will not result in decreased visibility impairment at Denali National Park.